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Interpolation-Based Immersed Finite Element and Isogeometric Analysis

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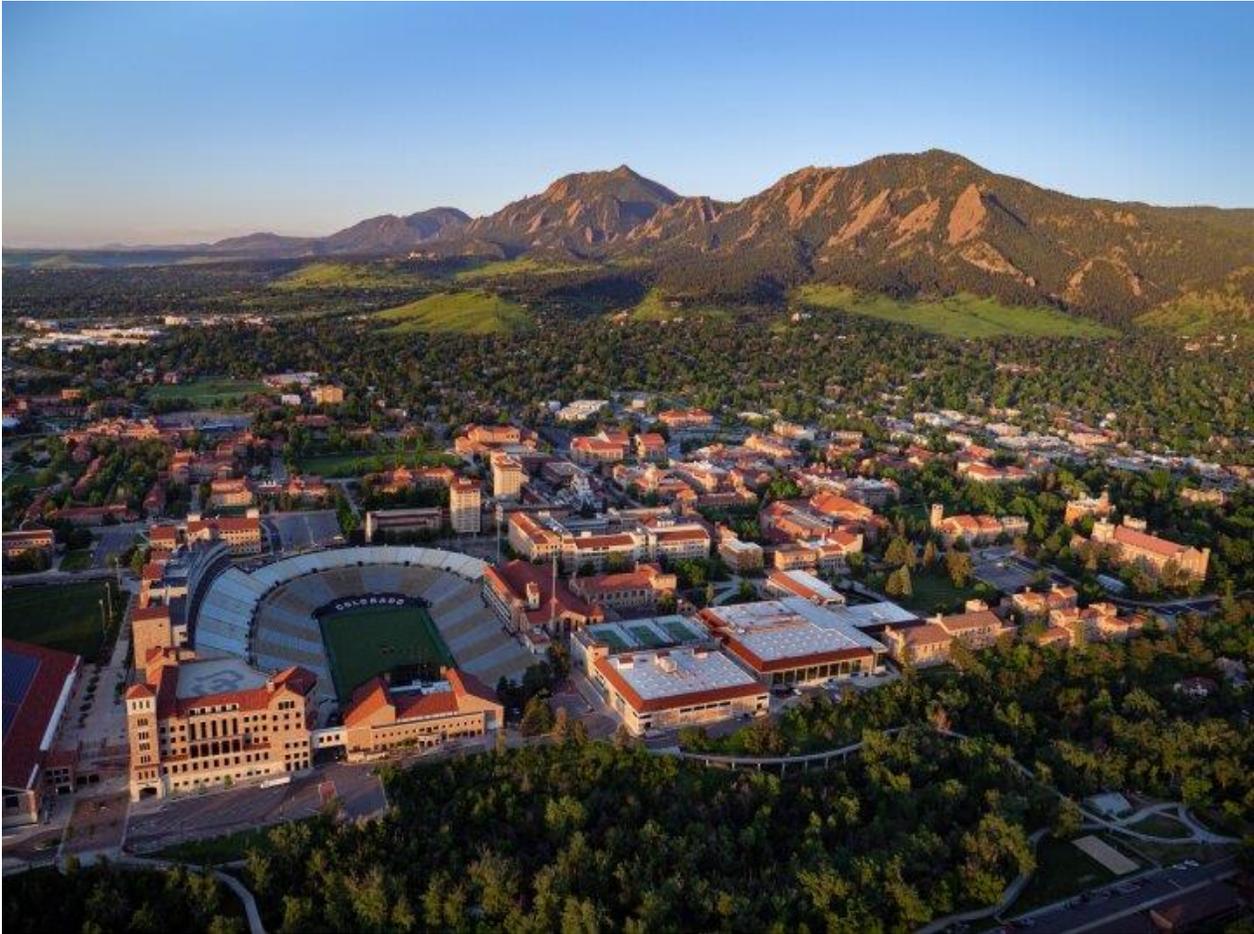
Ru Xiang



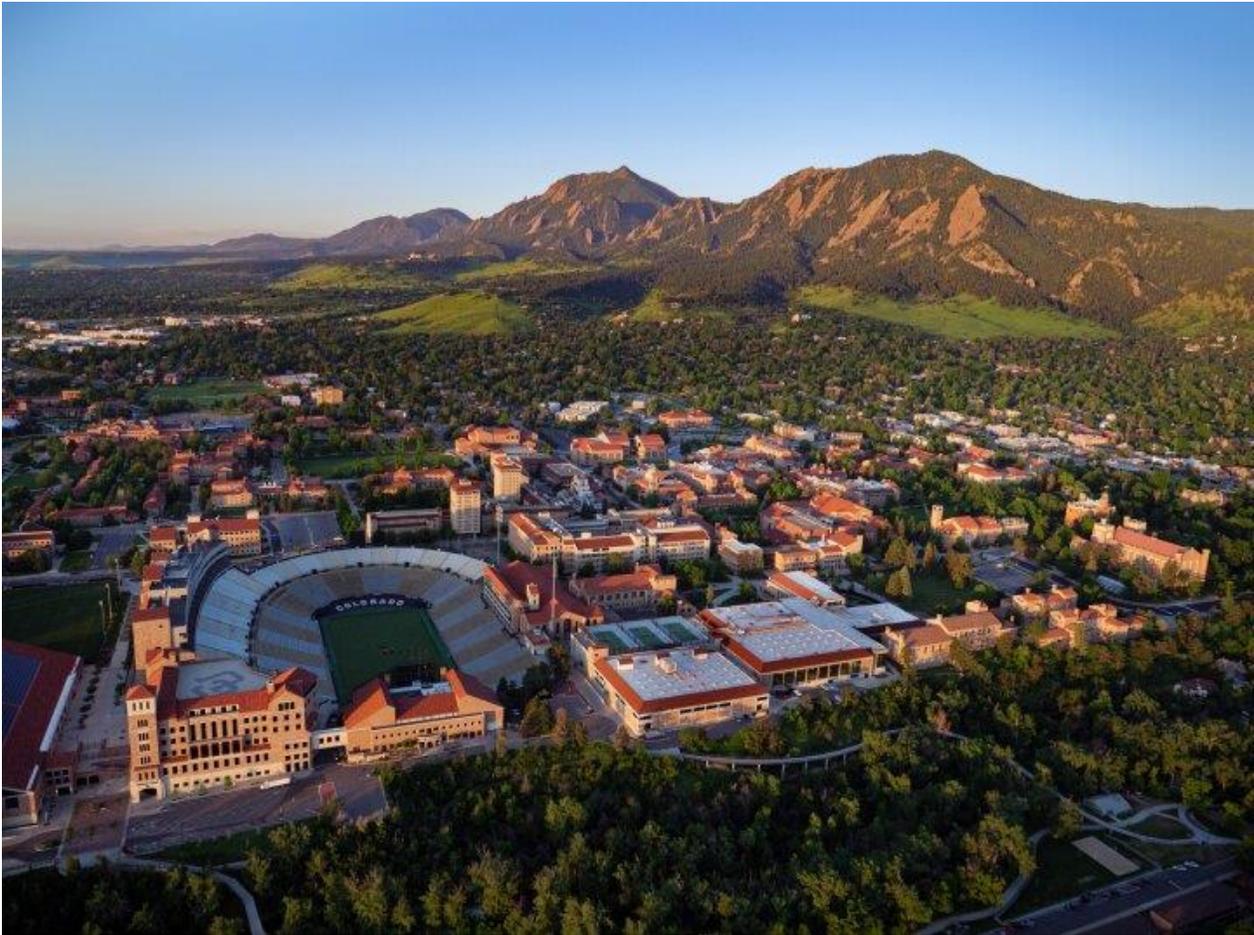
Han Zhao



Smead Aerospace Engineering Sciences at CU Boulder



Smead Aerospace Engineering Sciences at CU Boulder



Part 1:

Motivation

Motivation

Classical finite element analysis requires the generation of a **high quality body-fitted finite element mesh** which can require upwards of **80%** of the time required in a design-through-analysis cycle:

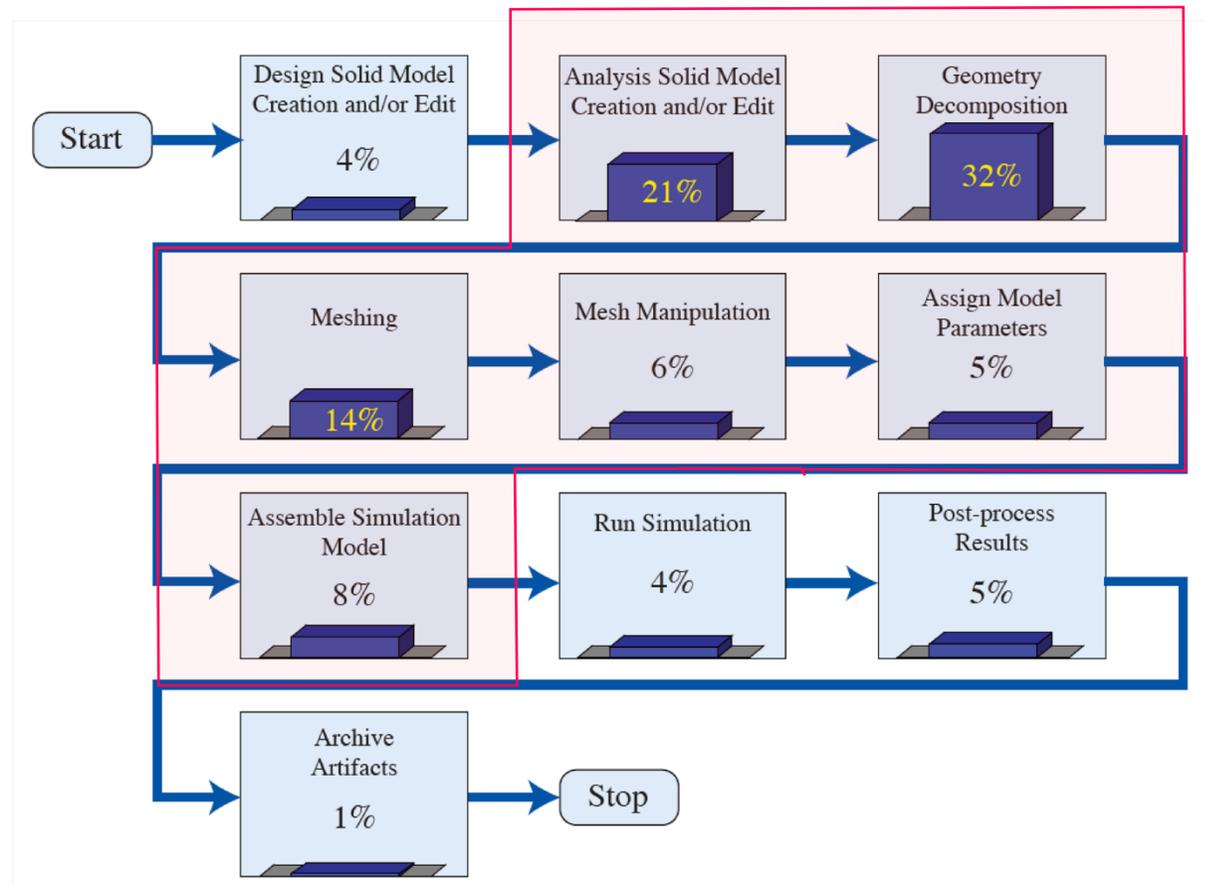
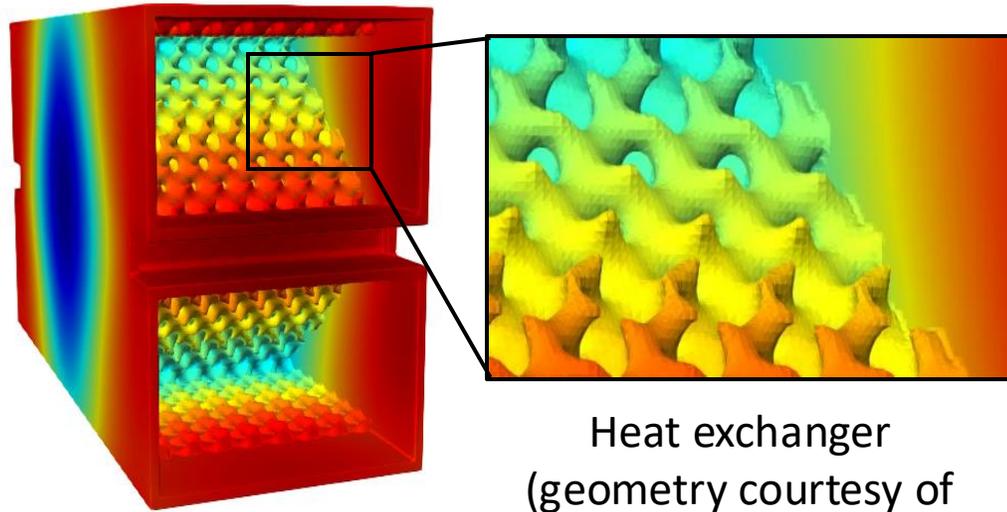


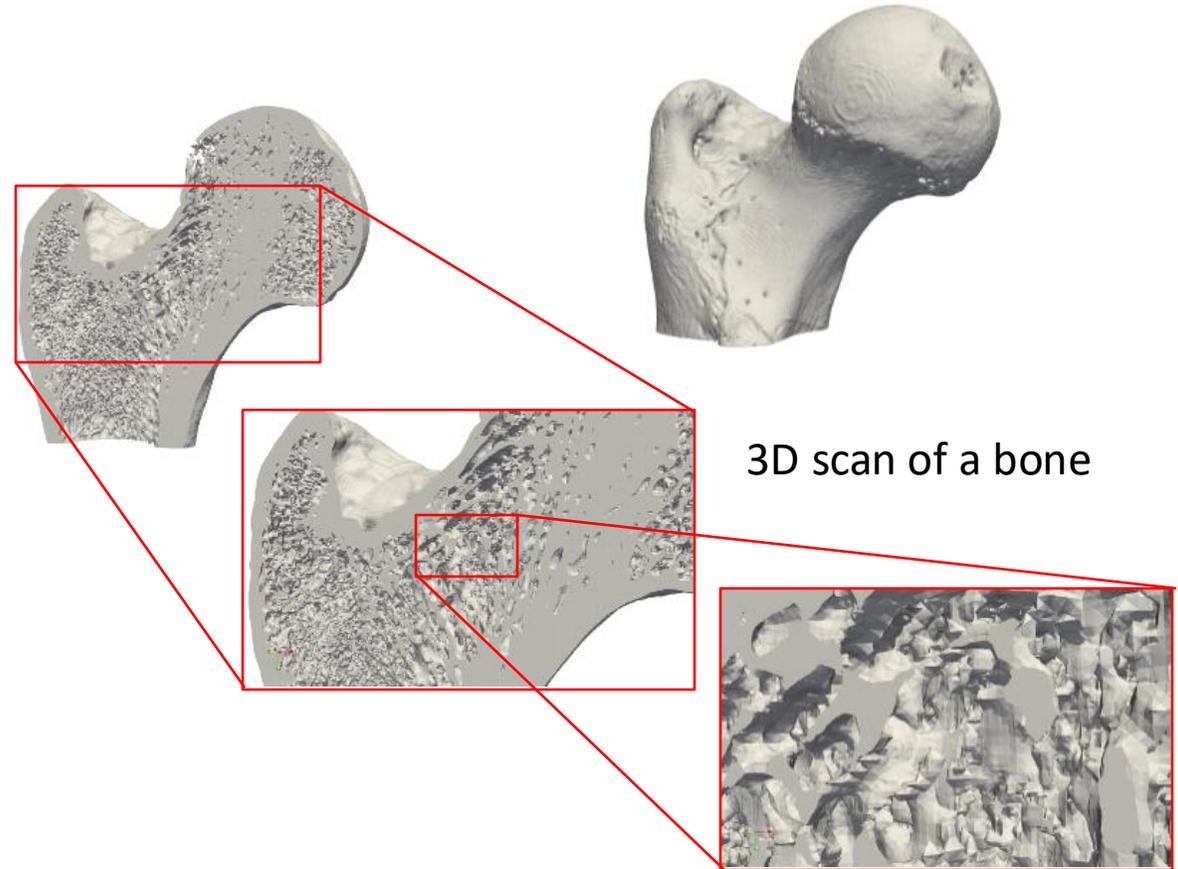
Figure courtesy of Sandia National Laboratories

Motivation

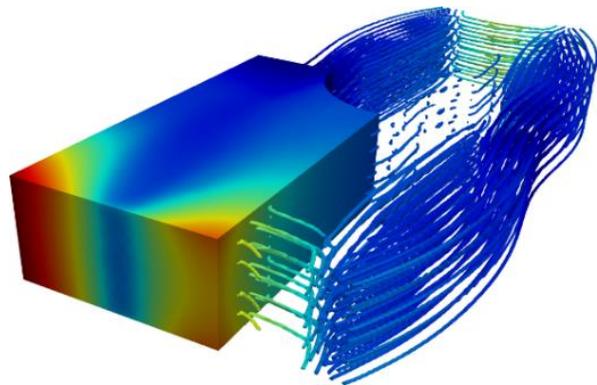
This is especially true for **geometrically complex, multi-material, multi-physics problems**:



Heat exchanger
(geometry courtesy of
nTopology)



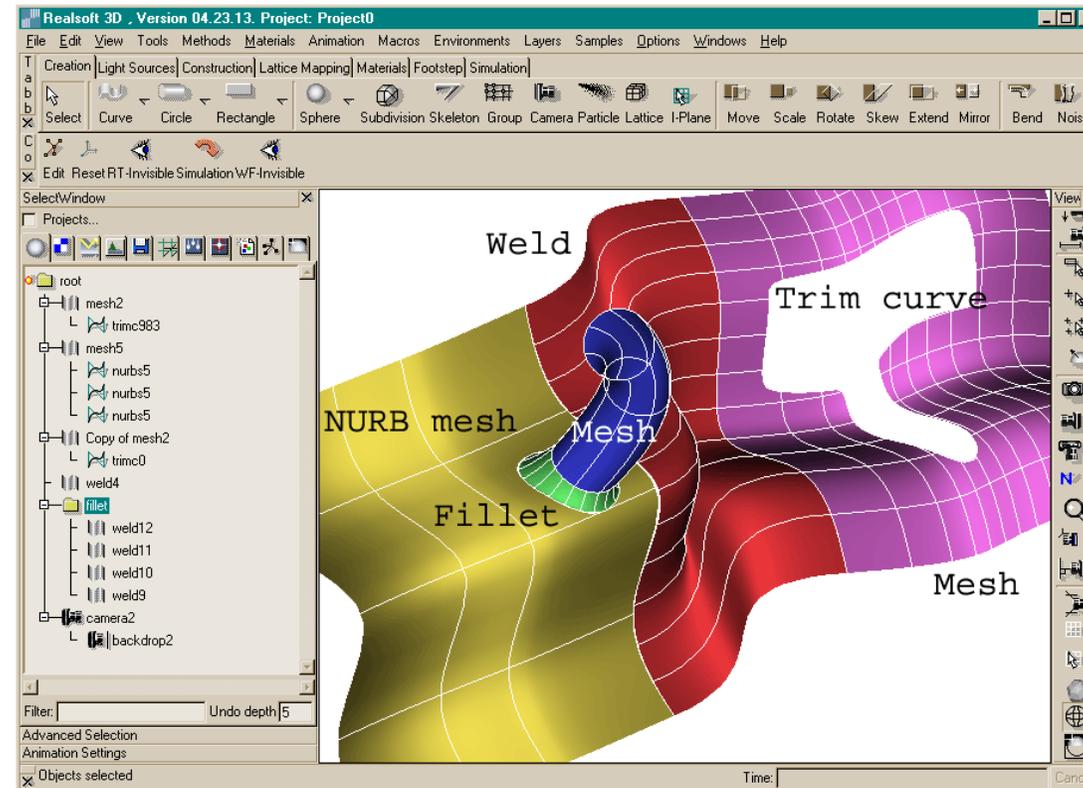
3D scan of a bone



Fiber composite

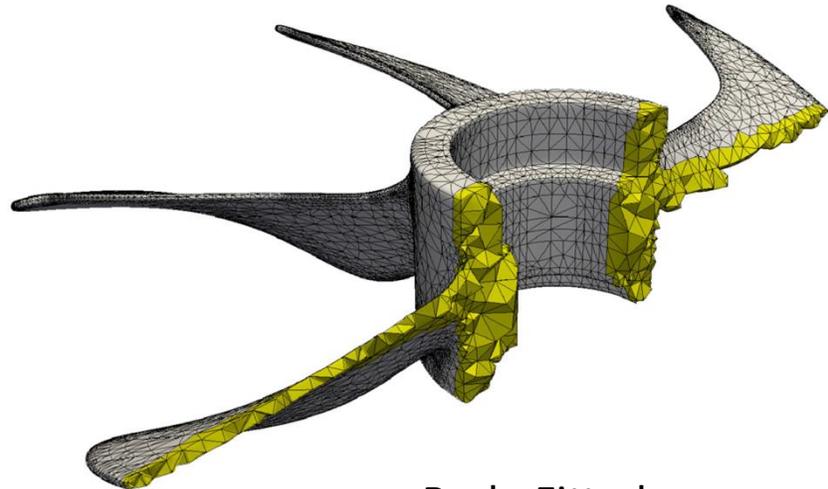
Motivation

Isogeometric analysis directly employs the basis employed in CAD for CAE and thus bypasses the need for the generation of a high quality body-fitted finite element mesh. However, isogeometric analysis requires an **explicit parameterization** of the geometric domain, and thus it cannot be directly applied to **trimmed CAD geometries**:

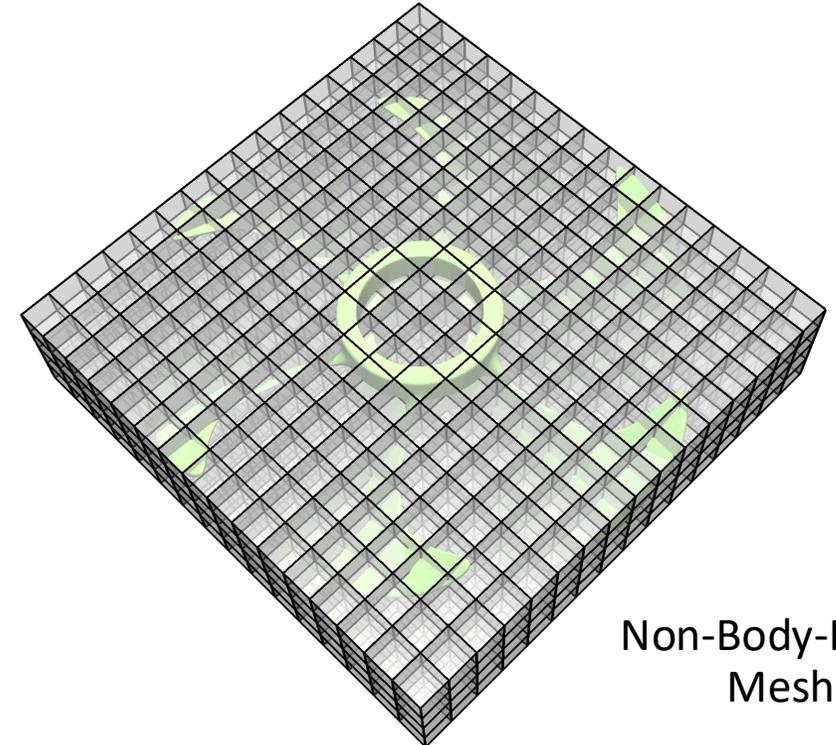
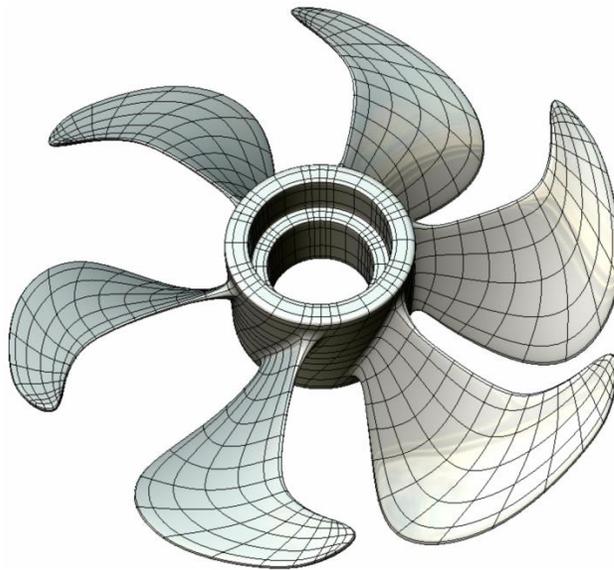


Motivation

Immersed finite element (and isogeometric) analysis is another approach that bypasses the need for the generation of a high quality body-fitted finite element mesh. In this approach, basis functions defined on a **non-body-fitted background mesh** are instead used for CAE, so it can be directly applied to trimmed CAD geometries:



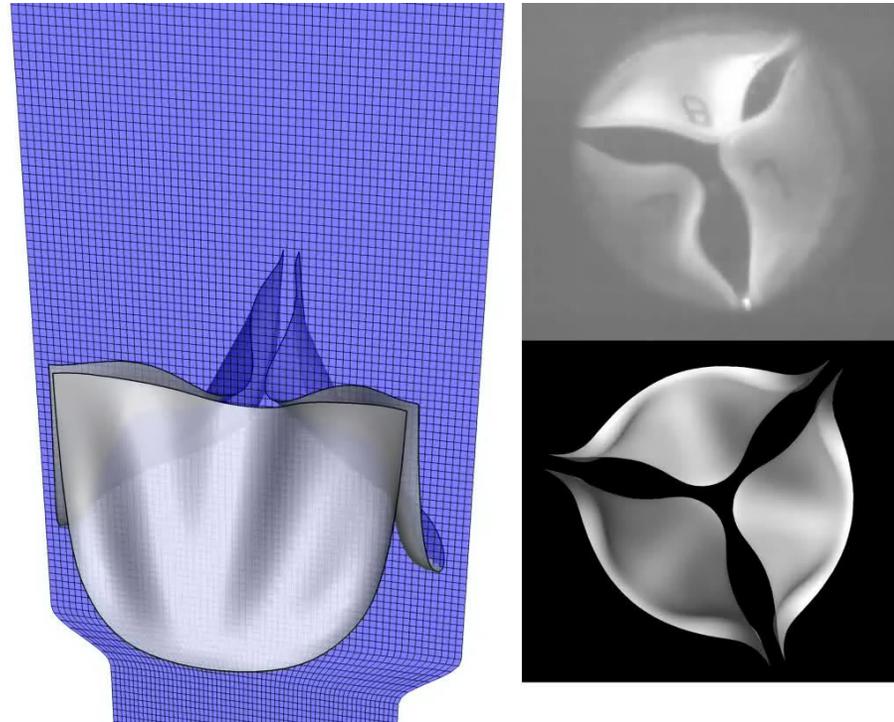
Body-Fitted
Mesh



Non-Body-Fitted
Mesh

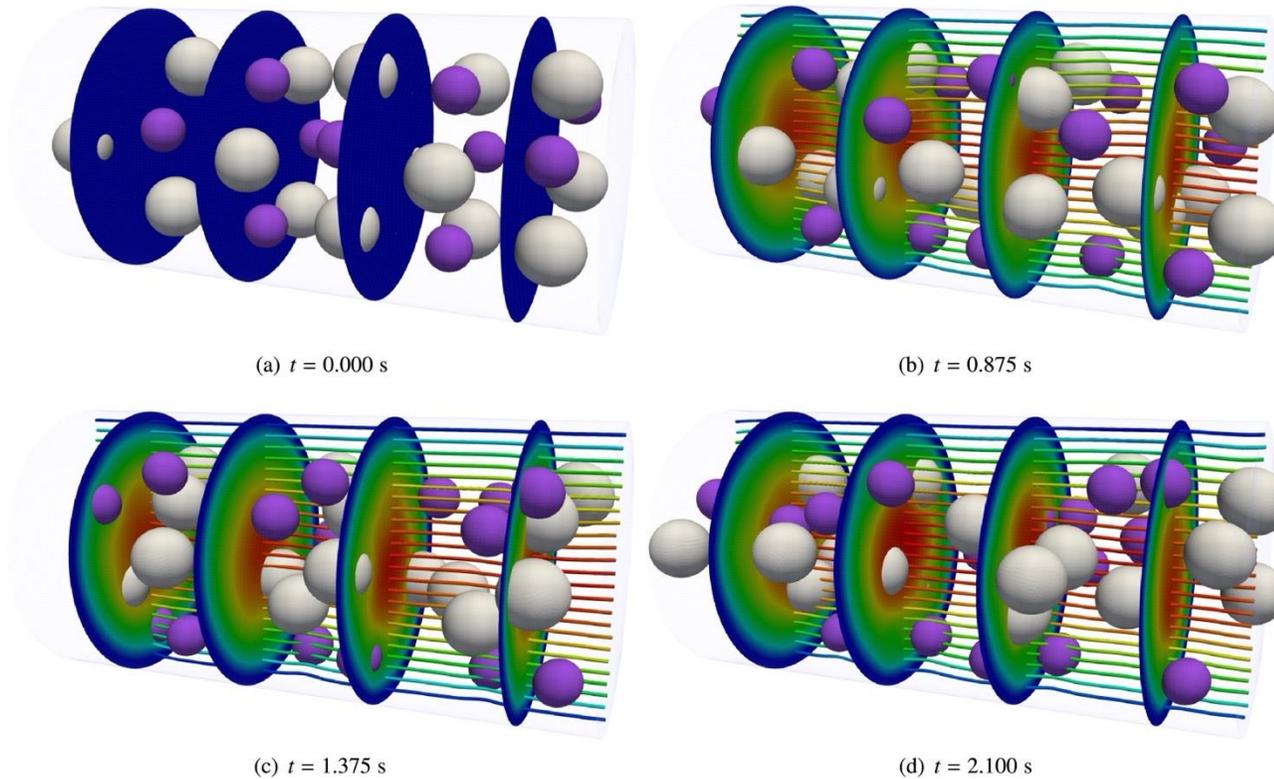
Motivation

Immersed finite element analysis can also be applied to problems out of reach by both classical finite element analysis and isogeometric analysis, such as problems exhibiting a **change in domain topology**:



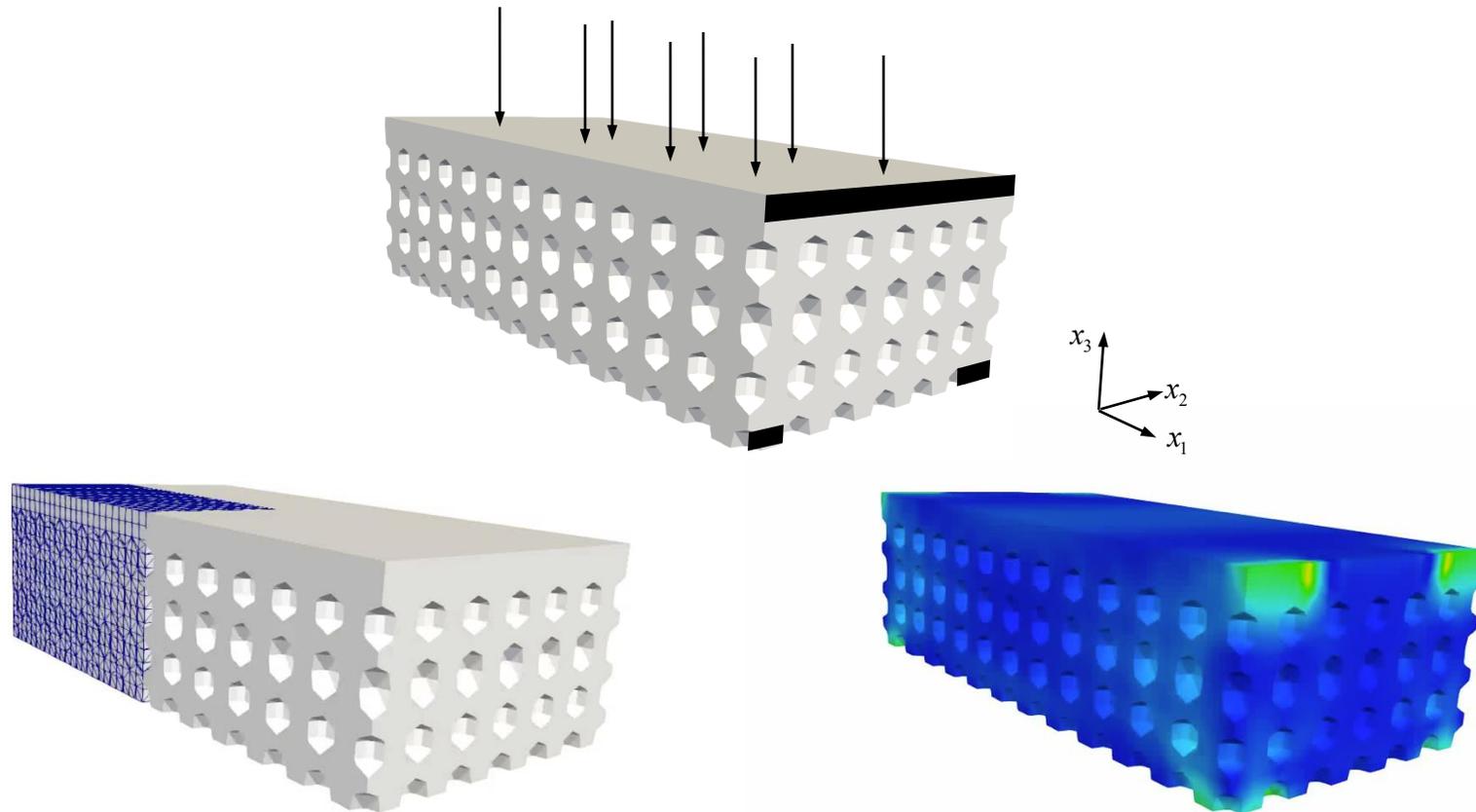
Motivation

Immersed finite element analysis can also be applied to problems out of reach by both classical finite element analysis and isogeometric analysis, such as problems exhibiting a **change in domain topology**:



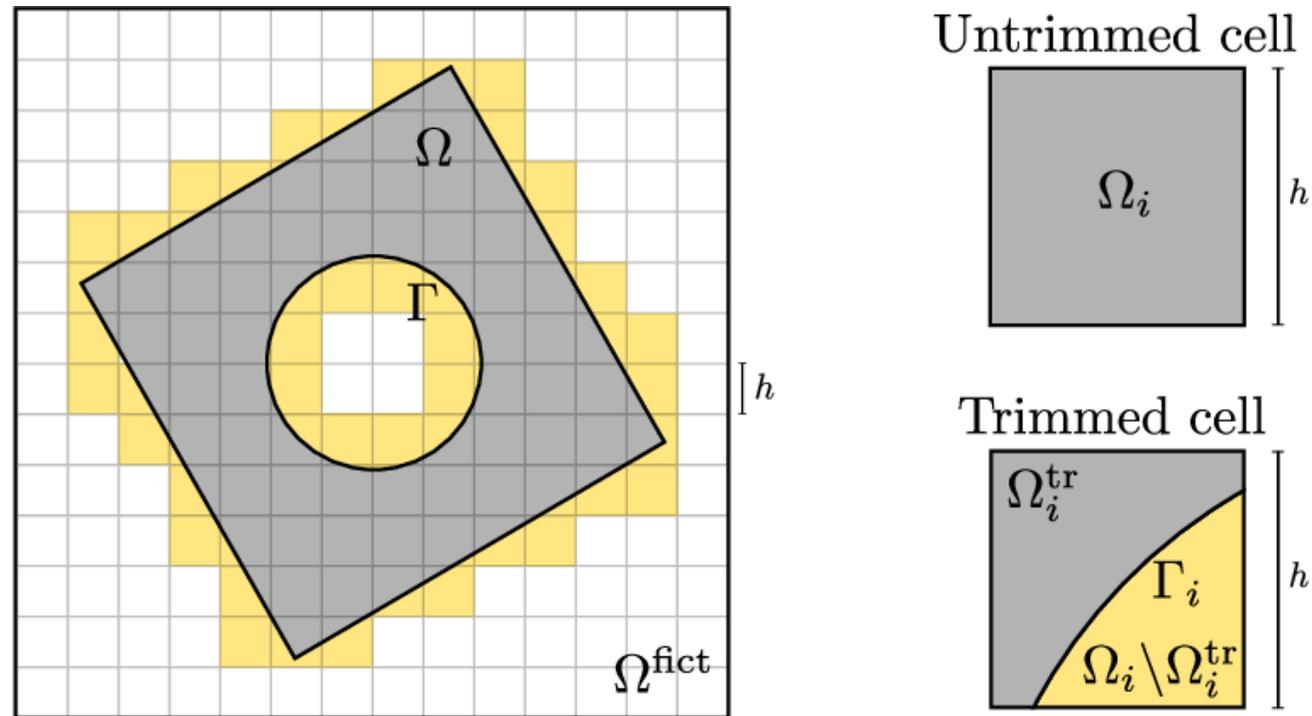
Motivation

Immersed finite element analysis is also an ideal technology for [level set topology optimization](#) as the geometric domain does not need to be re-parametrized or re-meshed at every design iteration:



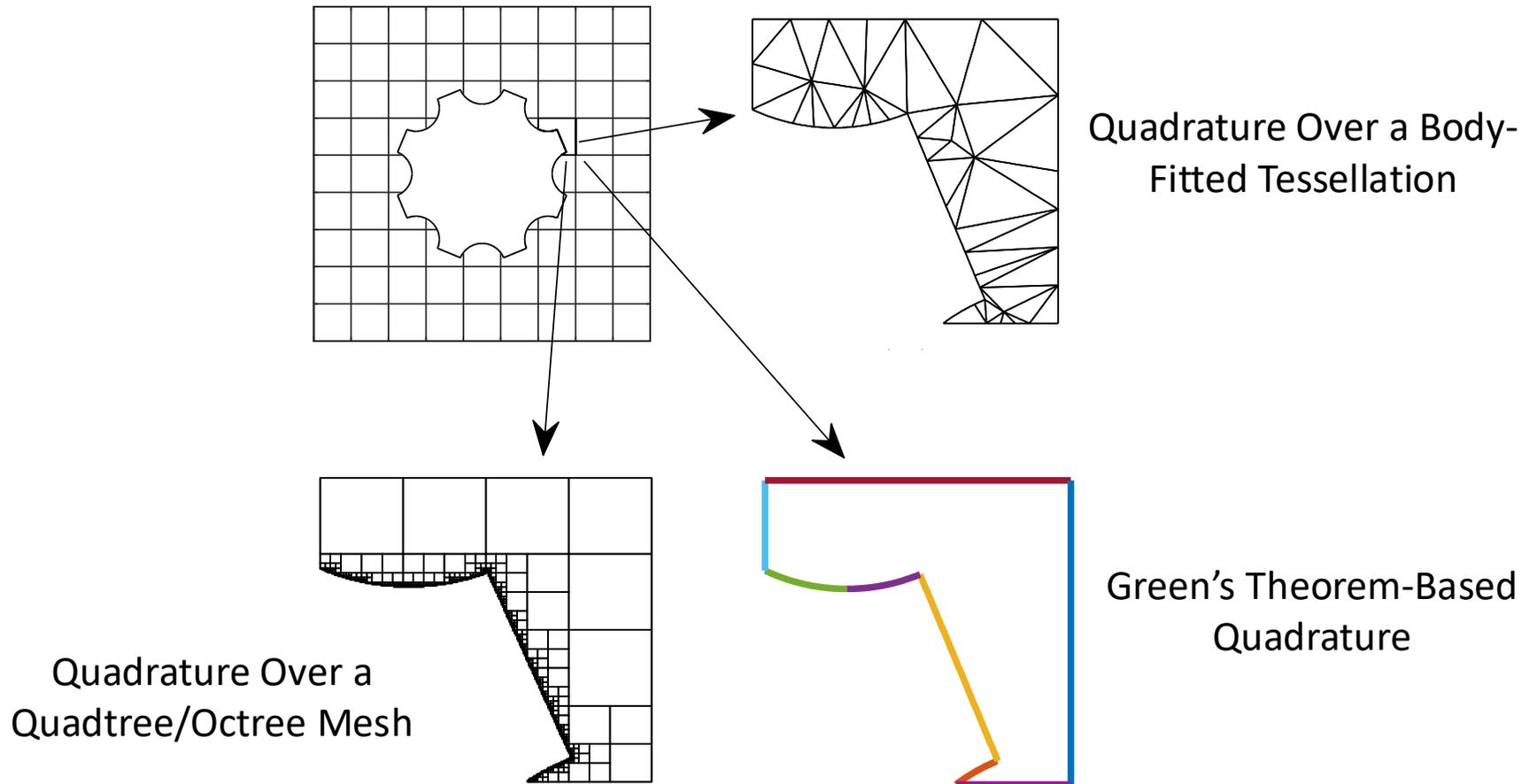
Motivation

However, **implementation** of an immersed finite element analysis code is a challenging and time consuming task even for domain experts. The primary challenge is **numerical integration over cut cells**:



Motivation

Several different strategies have been introduced for this integration, each giving rise to a **specialized quadrature rule** for **every single cut cell**:



Motivation

The purpose of the [EXHUME project](#) is to [ease the burden](#) of implementing an immersed finite element code.

In particular, the EXHUME project enables one to [transform classical finite element codes](#) into immersed finite element codes with [minimal implementation effort](#).

The key technology underlying the EXHUME project is the concept of [interpolation-based immersed finite element analysis](#).

Part 2:

Interpolation-Based Immersed Finite Element Analysis

Defining the Method for a Model Problem

- Use **Poisson equation** as model PDE for exposition

- Strong form: Find solution u s.t.

$$-\Delta u = f \quad \text{in } \Omega$$

$$u = g \quad \text{on } \partial\Omega$$

- Weak form: Find $u \in H_0^1(\Omega) + \ell_g$ s.t. $\forall v \in H_0^1(\Omega)$

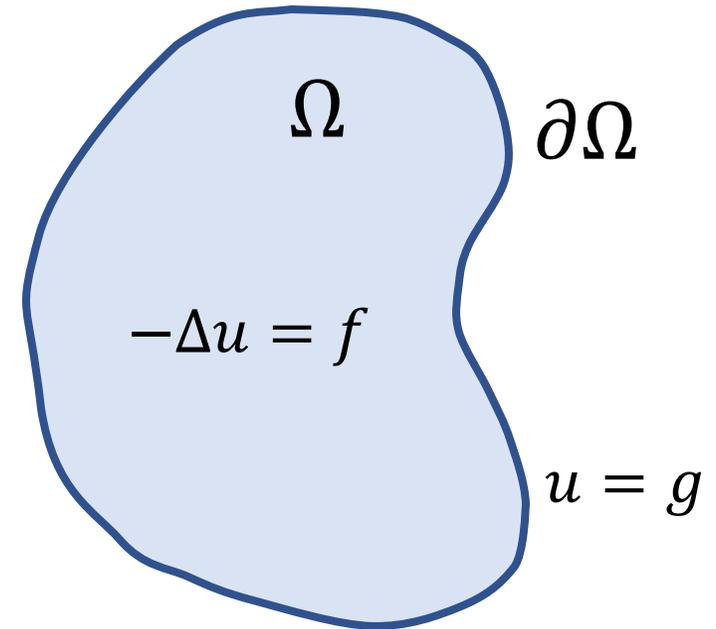
$$\int_{\Omega} \nabla u \cdot \nabla v \, d\Omega = \int_{\Omega} f v \, d\Omega$$

- Discrete problem: Find $u^h \in V^h \subset H^1(\Omega)$ s.t. $\forall v^h \in V^h$

$$\int_{\Omega} \nabla u^h \cdot \nabla v^h \, d\Omega - \int_{\partial\Omega} \nabla u^h \cdot \mathbf{n} v^h \, d\Gamma$$

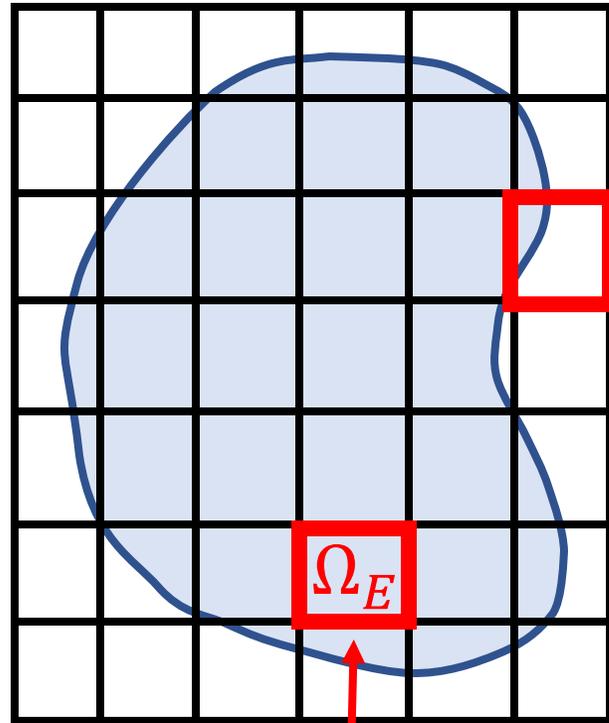
$$\mp \int_{\partial\Omega} \nabla v^h \cdot \mathbf{n} (u^h - g) \, d\Gamma$$

$$+ \int_{\partial\Omega} \frac{\alpha}{h} (u^h - g) v^h \, d\Gamma = \int_{\Omega} f v^h \, d\Omega$$



Using Nitsche's method for weak enforcement of Dirichlet BCs

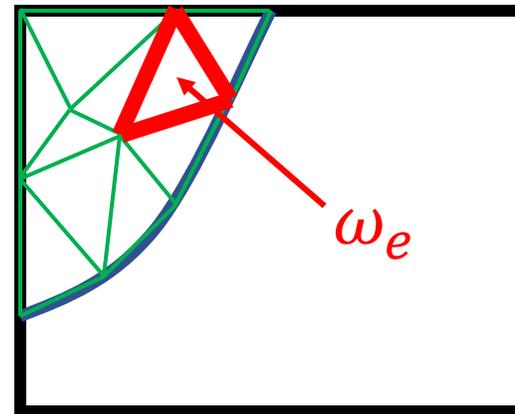
Quadrature-Based Immersed Methods



Define V^h on **background mesh**

Challenge: Integrate accurately over intersections of domain with **cut cells**

Can use standard element Gaussian quadrature on cells contained in Ω



Solution: Tessellate mesh-cell intersections with quadrature elements, forming a **foreground mesh**

Can use standard Gaussian quadrature on elements of foreground mesh

In Mathematical Notation:

Discrete problem is: Find $u^h \in V^h$ s.t. $\forall v^h \in V^h$,

$$a_h(u^h, v^h) = L_h(v^h),$$

where

$$a_h(u, v) := \sum_{e=1}^{vel} \int_{\omega_e} \nabla u \cdot \nabla v \, d\Omega + \sum_{e=1}^{vel} \int_{\partial\omega_e \cap \partial\Omega} -v \nabla u \cdot \mathbf{n} \mp u \nabla v \cdot \mathbf{n} + \left(\frac{\alpha}{h}\right) uv \, d\Gamma,$$

$$L_h(v) := \sum_{e=1}^{vel} \int_{\omega_e} f v \, d\Omega + \sum_{e=1}^{vel} \int_{\partial\omega_e \cap \partial\Omega} \mp g \nabla v \cdot \mathbf{n} + \left(\frac{\alpha}{h}\right) gv \, d\Gamma,$$

$\{\omega_e\}_{e=1}^{vel}$ are **elements of the foreground mesh**, and the discrete space is

$$V^h := \text{span}\{N_i|_{\Omega}\}_{i=1}^n$$

with basis functions $\{N_i\}_{i=1}^n$ **defined on the background mesh**.

Implementation problem: Quadrature defined on foreground mesh, but basis functions defined on background mesh; cannot use standard FEM data structures and assembly algorithms!

Interpolation-Based Immersed Methods

Want: Basis functions used for assembly defined on the same mesh as the quadrature rule.

Approach:

- Define nodal basis on foreground mesh: $\{\phi_j\}_{j=1}^v$ with nodes $\{\mathbf{x}_j\}_{j=1}^v$
- Interpolate background basis functions in foreground space: $\widehat{N}_i = \sum_{j=1}^v N_i(\mathbf{x}_j)\phi_j$
- Use span of interpolated background basis functions as solution space: $V^h = \text{span}\{\widehat{N}_i\}_{i=1}^n$

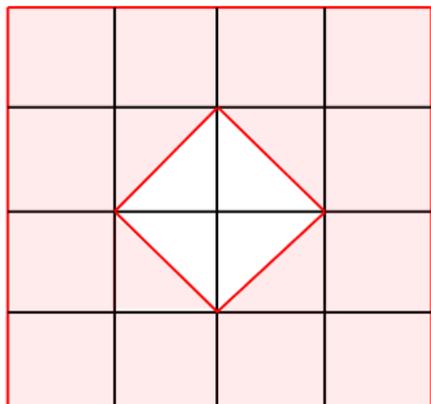
Equivalent to quadrature-based method *if*:

- Foreground mesh fitted to background mesh
- Foreground basis can exactly represent all monomials in background basis functions

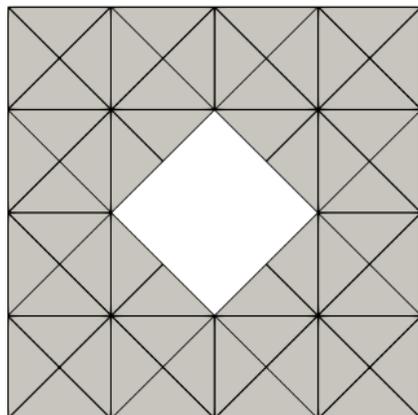
Possible approximations (new numerical methods):

- Reduced polynomial degree of foreground basis \Rightarrow More efficient assembly
- Background-unfitted foreground mesh \Rightarrow More flexibility in mesh generation

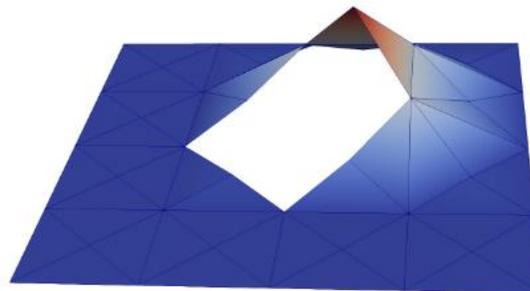
Interpolated Basis Functions



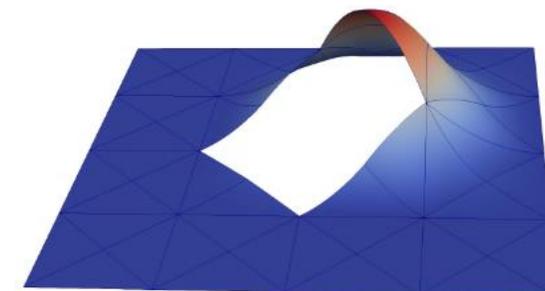
Domain in red,
background mesh in black



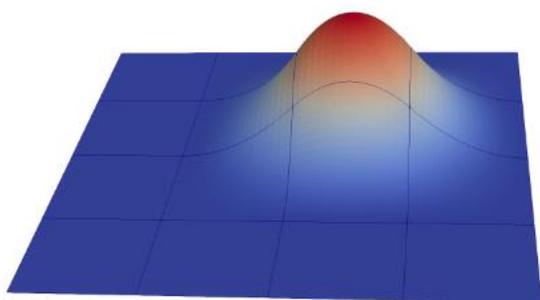
“Background-fitted”
foreground mesh



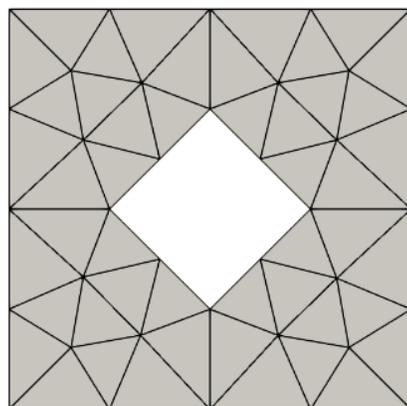
\widehat{N}_i for piecewise-linear Lagrange
foreground basis $\{\phi_j\}$



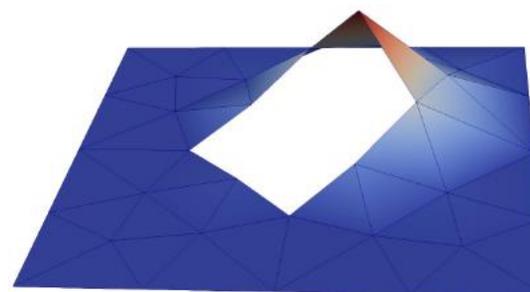
\widehat{N}_i for piecewise-quadratic
Lagrange foreground basis $\{\phi_j\}$



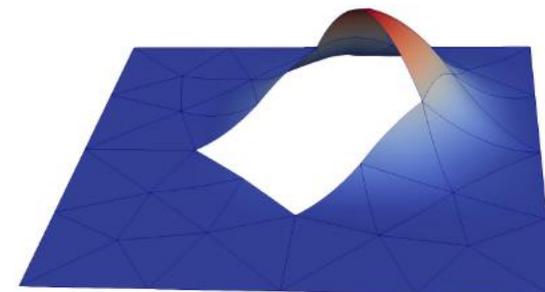
C^1 quadratic B-spline
background basis function N_i



“Background-unfitted”
foreground mesh



\widehat{N}_i for piecewise-linear Lagrange
foreground basis $\{\phi_j\}$



\widehat{N}_i for piecewise-quadratic
Lagrange foreground basis $\{\phi_j\}$

Implementation Using an Existing FE Code

Matrix notation for discrete problem we want to solve:

$$\mathbf{Kd} = \mathbf{F}, \text{ where } K_{ij} = a_h(\widehat{N}_j, \widehat{N}_i) \text{ and } F_i = L_h(\widehat{N}_i).$$

What is easy to assemble over the foreground mesh with an existing FE code:

$$A_{ij} = a_h(\phi_j, \phi_i) \text{ and } B_i = L_h(\phi_i).$$

Transformation to desired problem, using standard linear algebra routines (e.g., backend library):

$$\mathbf{K} = \mathbf{M}^T \mathbf{A} \mathbf{M} \text{ and } \mathbf{F} = \mathbf{M}^T \mathbf{B},$$

where $M_{ij} = N_j(\mathbf{x}_i)$.

Only non-standard assumption: Existing FE code can implement a_h and L_h for Nitsche's method.

Interpolation Error Bound

For background-fitted foreground meshes, and under various technical assumptions, we have the interpolation bound

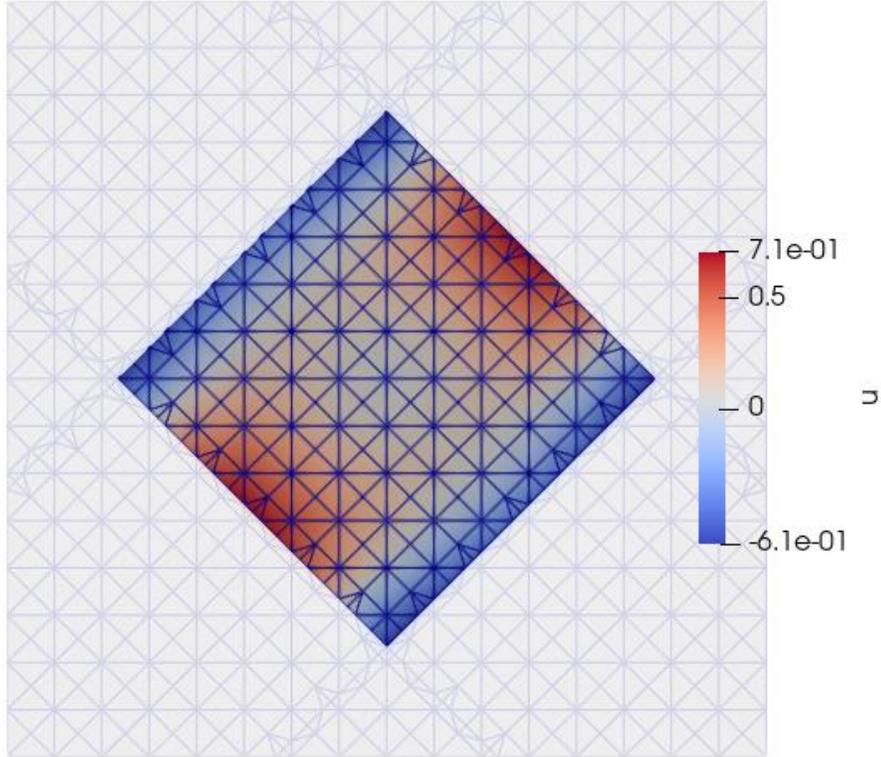
$$v^h \in \text{span}\{\widehat{N}_i\} \quad \|u - v^h\|_{H^1(\Omega)} \leq Ch^{\widehat{k}} \|u\|_{H^{\widehat{k}+1}(\Omega)}$$

where $\widehat{k} = \min\{k, \kappa\}$ is the minimum degree of polynomial completeness between the background (k) and foreground (κ) function spaces.

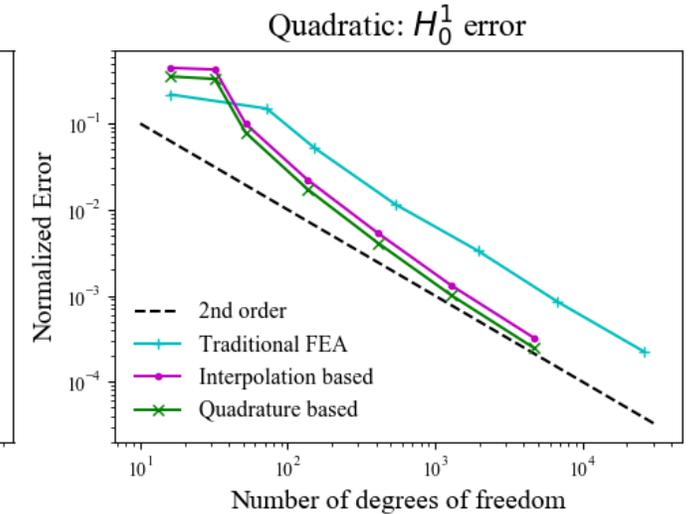
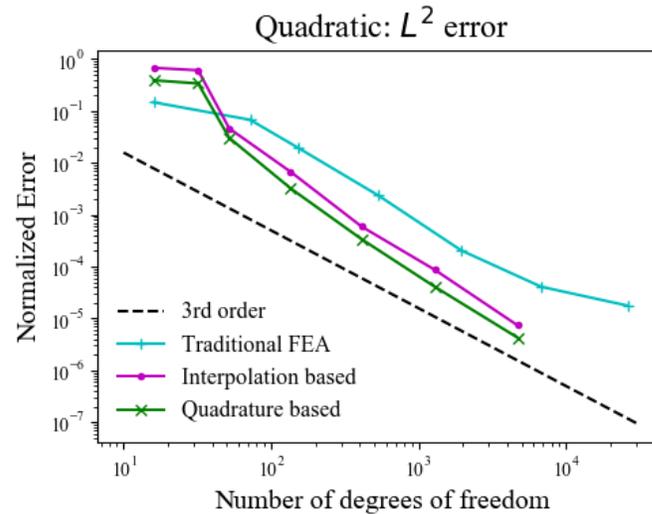
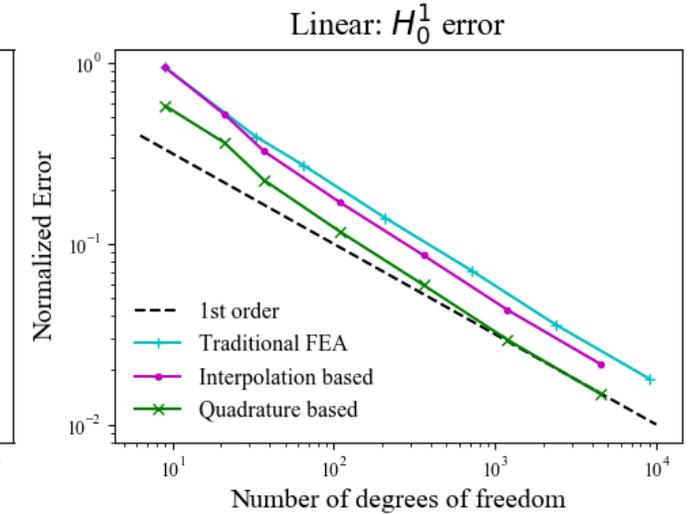
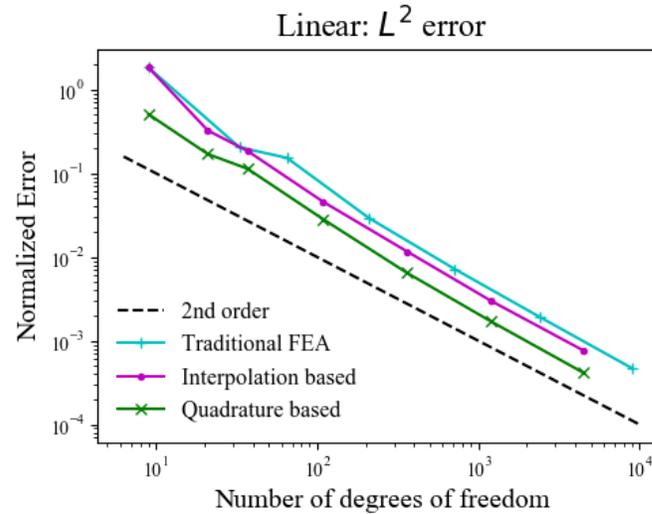
Note: Background space may have some monomials with degree $\geq k$; these do not need to be captured in foreground space for optimal-order interpolation error.

Numerical results suggest that this holds under significantly more general conditions.

Results: 2D Poisson with Background-*Fitted* Foreground Mesh

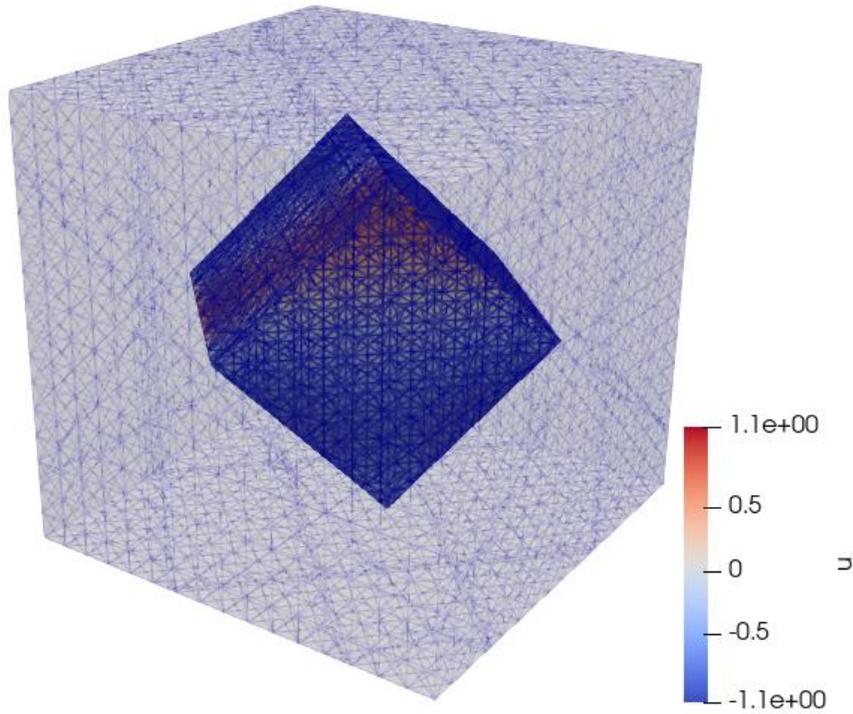


Convergence testing using a manufactured solution to Poisson's equation

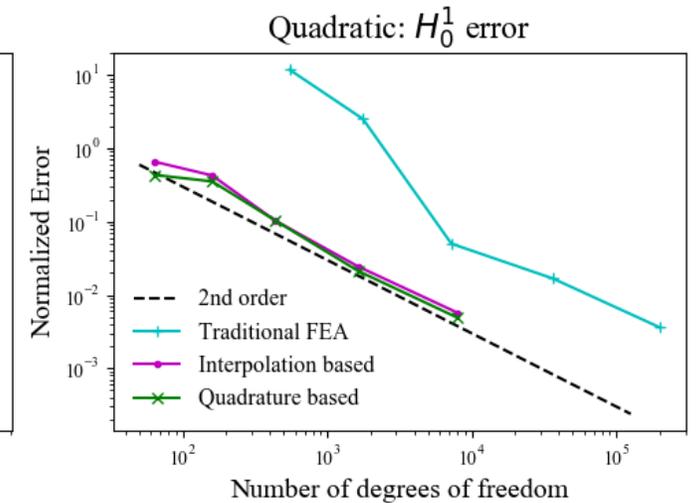
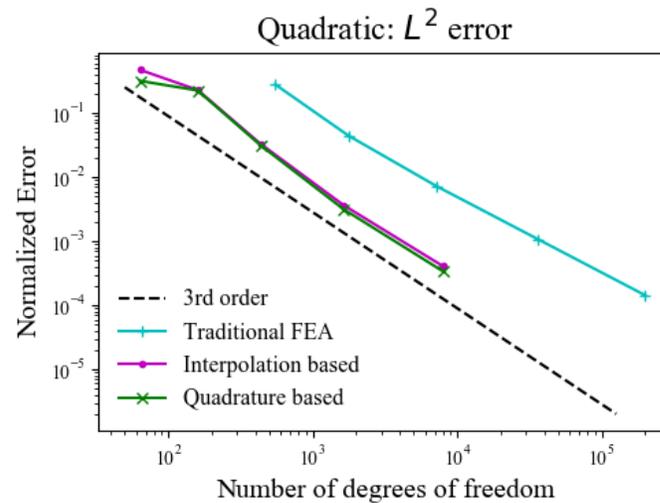
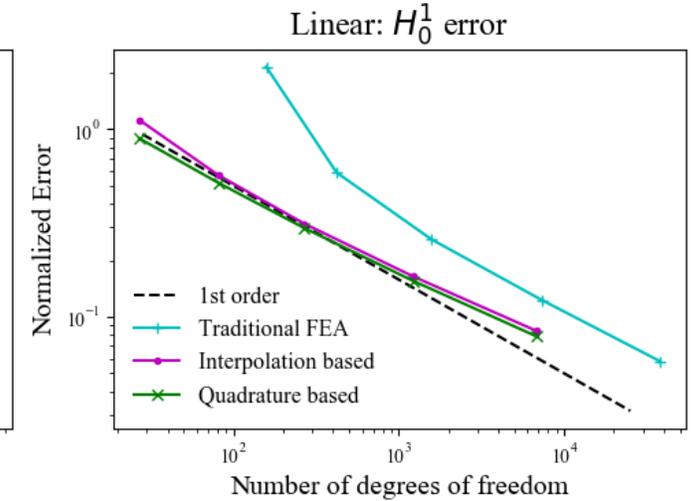
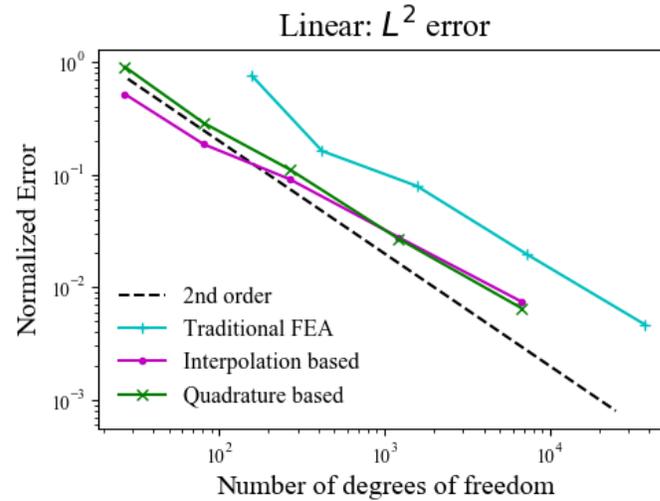


Convergence at optimal rates

Results: 3D Poisson with Background-*Fitted* Foreground Mesh

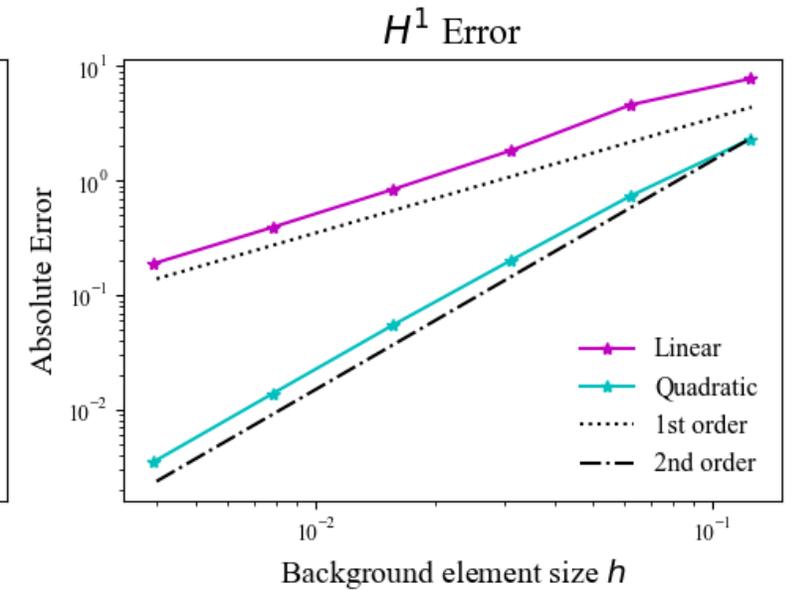
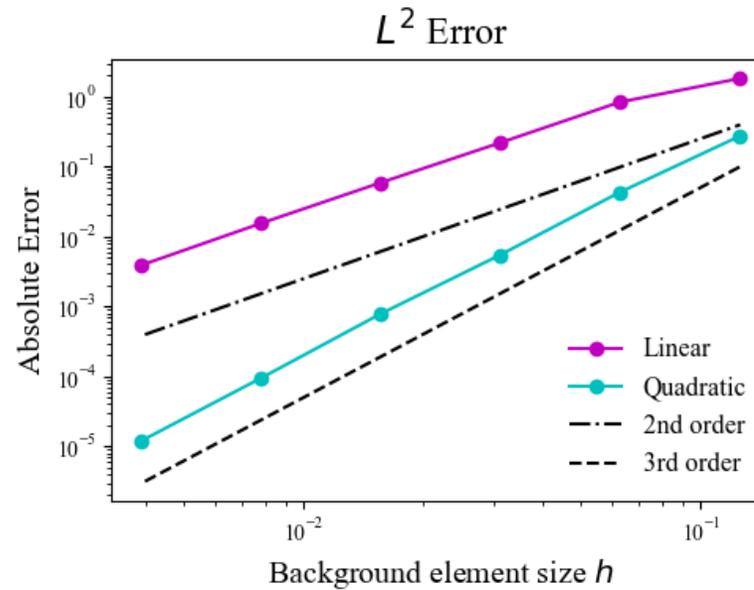
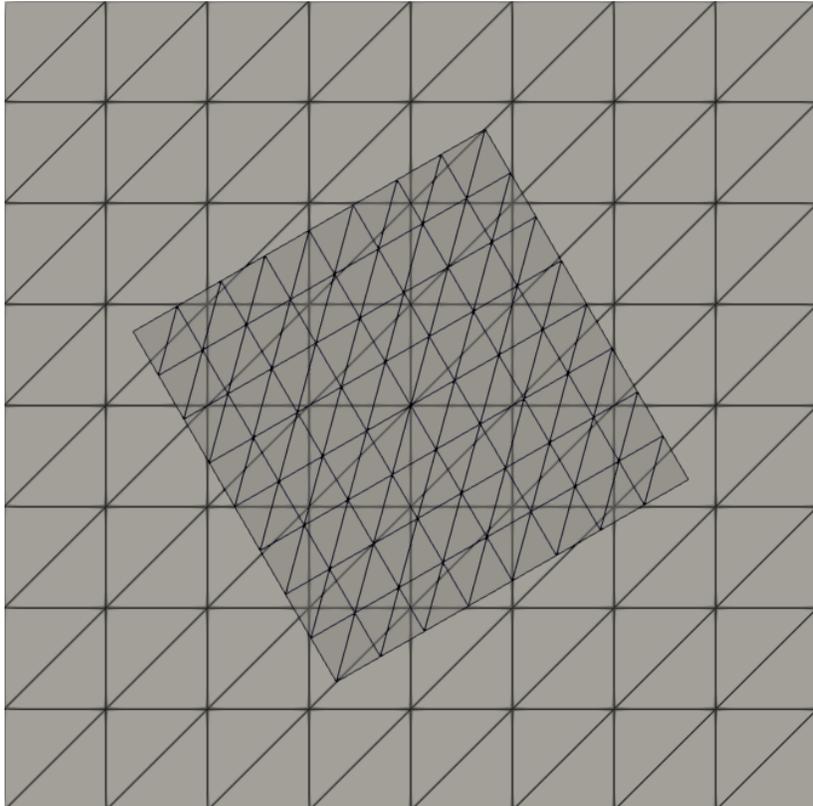


Convergence testing using a manufactured solution to Poisson's equation



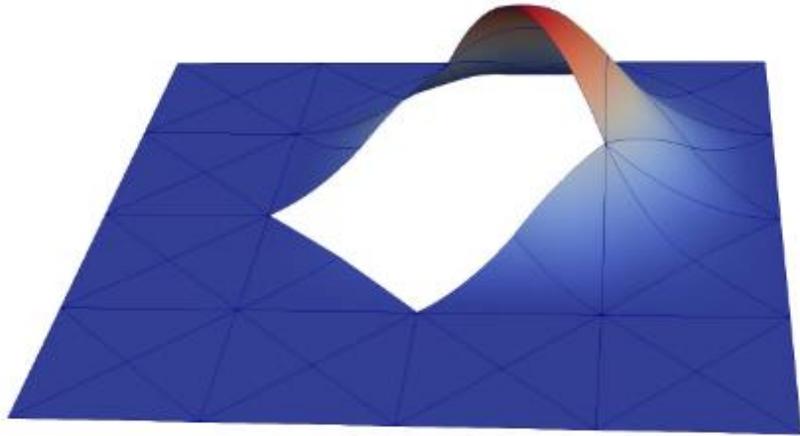
Convergence at optimal rates

Results: 2D Poisson with Background-*Unfitted* Foreground Mesh

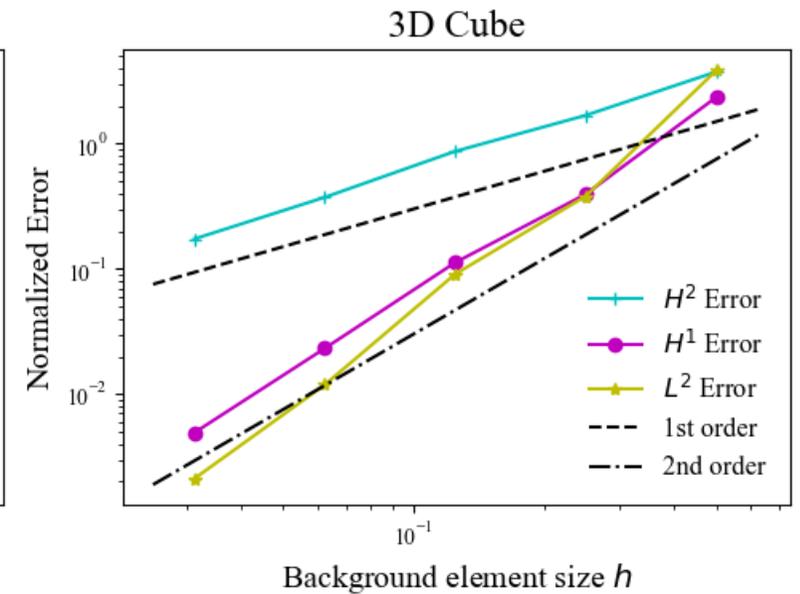
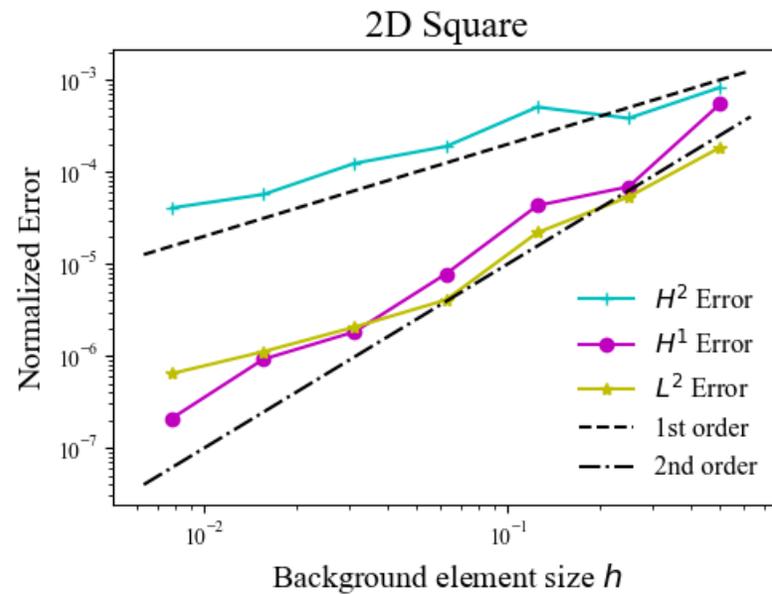


Still converging at optimal rates, but outside the scope of our initial interpolation error analysis.

Results: Biharmonic (non-conforming!)

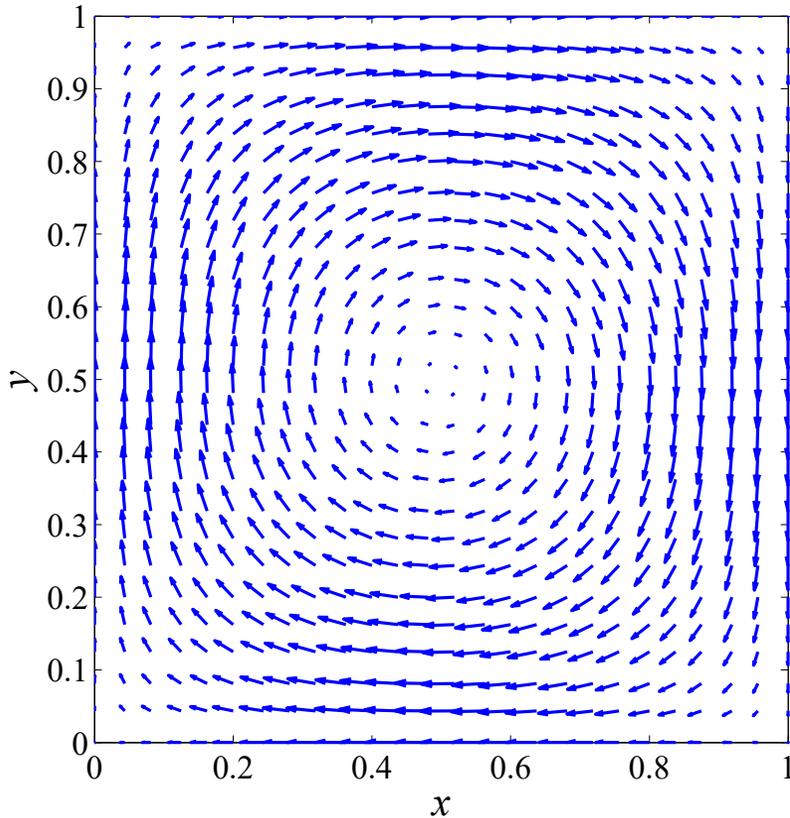


Note: Quadratic Lagrange interpolation of a C^1 quadratic B-spline function is not exactly C^1 , and thus not $\in H^2(\Omega)$!



Still obtain convergence rates expected from theory for conforming formulation.

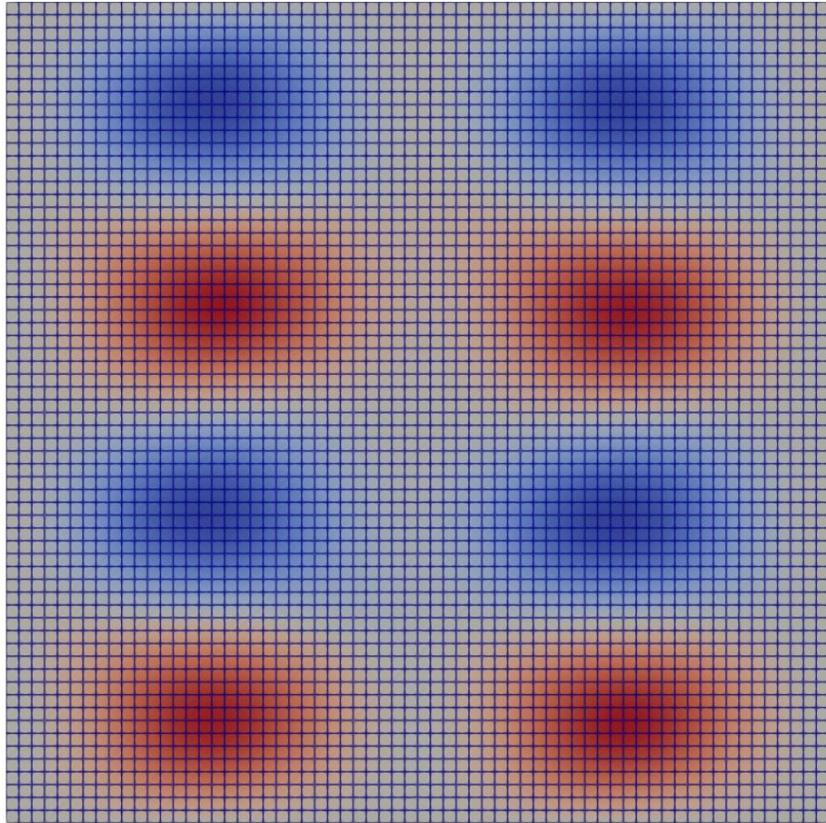
Interpolation-Based Isogeometric Analysis of Navier-Stokes Flow Using Equal-Order Elements and VMS Stabilization



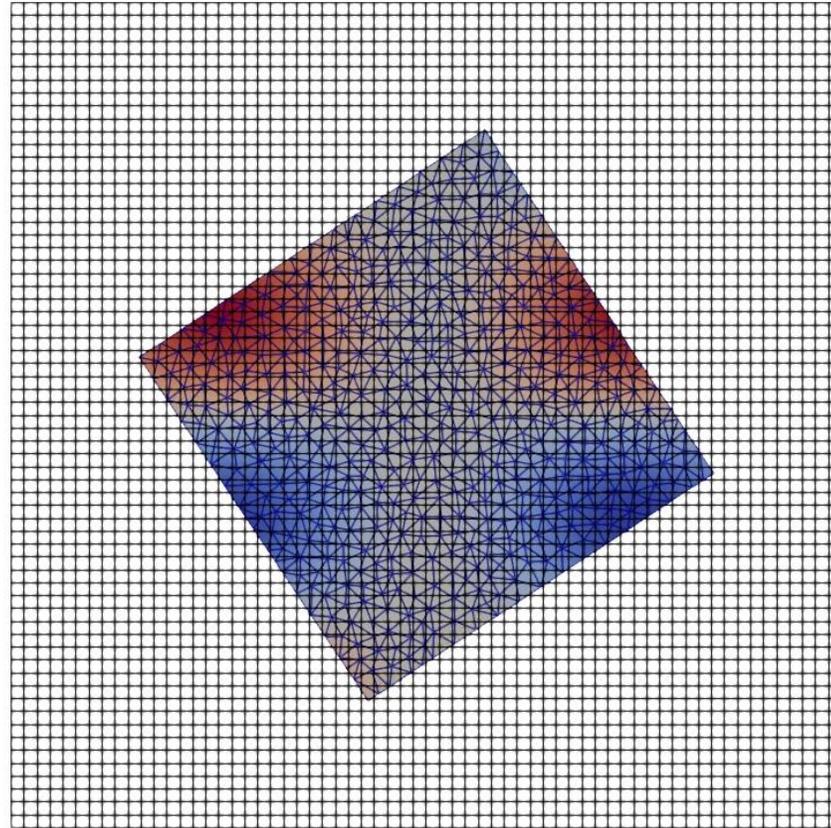
Taylor-Green Vortex at $Re = 100$

$$\begin{aligned}
 & \int_{\Omega} (\rho (\partial_t \mathbf{u}^h + \mathbf{u}^h \cdot \nabla \mathbf{u}^h) \cdot \mathbf{v}^h + \boldsymbol{\sigma}(\mathbf{u}^h, p^h) : \nabla \mathbf{v}^h + \nabla \cdot \mathbf{u}^h q^h) d\Omega \\
 & + \int_{\partial\Omega} (-(\boldsymbol{\sigma}(\mathbf{u}^h, p^h) \mathbf{n}) \cdot \mathbf{v}^h + (\boldsymbol{\sigma}(\mathbf{v}^h, q^h) \cdot \mathbf{n}) \cdot (\mathbf{u}^h - \mathbf{g})) d\Gamma \\
 & \quad - \int_{\partial\Omega} (\rho \min\{\mathbf{u}^h \cdot \mathbf{n}, 0\} (\mathbf{u}^h - \mathbf{g}) \cdot \mathbf{v}^h) d\Gamma \\
 & + \int_{\Omega} \tau_M \left(\left(\mathbf{u}^h \cdot \nabla \mathbf{v}^h + \frac{1}{\rho} \nabla q^h \right) \cdot \mathbf{r}_M - \mathbf{v}^h \cdot \mathbf{r}_M \cdot \nabla \mathbf{u}^h \right) d\Omega \\
 & \quad - \int_{\Omega} \frac{\tau_M^2}{\rho} (\nabla \mathbf{v}^h) : (\mathbf{r}_M \otimes \mathbf{r}_M) d\Omega \\
 & + \int_{\Omega} \tau_C (r_C \nabla \cdot \mathbf{v}^h) d\Omega = 0
 \end{aligned}$$

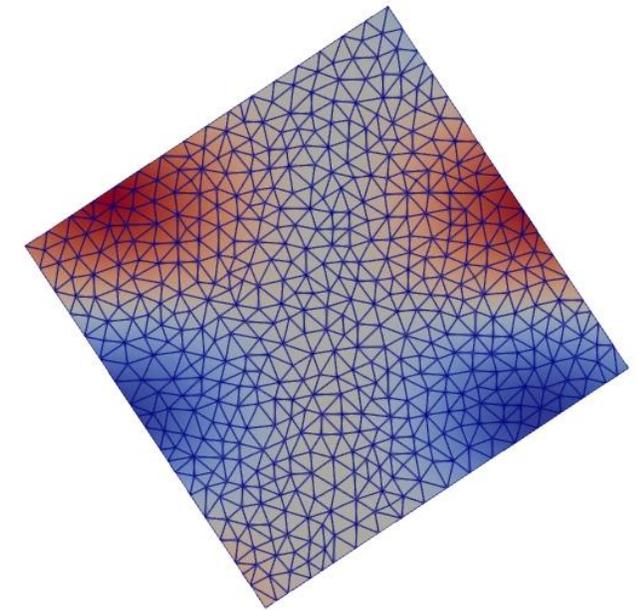
Interpolation-Based Isogeometric Analysis of Navier-Stokes Flow Using Equal-Order Elements and VMS Stabilization



BG Mesh with Exact Solution
(Tensor Product Spline Space)



BG Mesh with
Overlaying FG Mesh



FG Mesh

Interpolation-Based Isogeometric Analysis of Navier-Stokes Flow Using Equal-Order Elements and VMS Stabilization

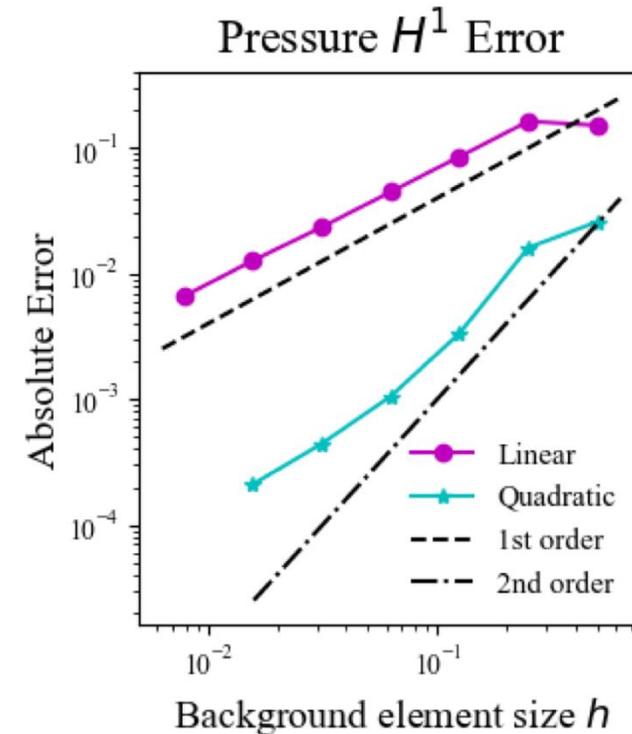
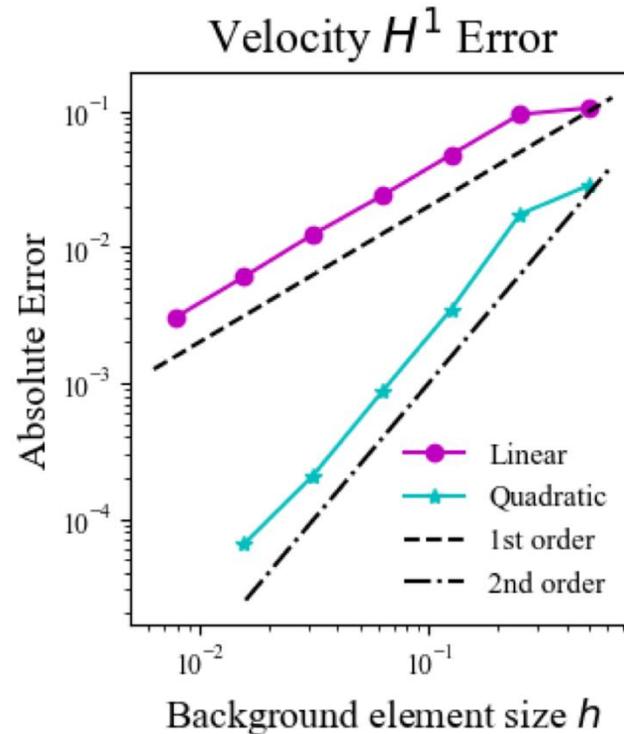
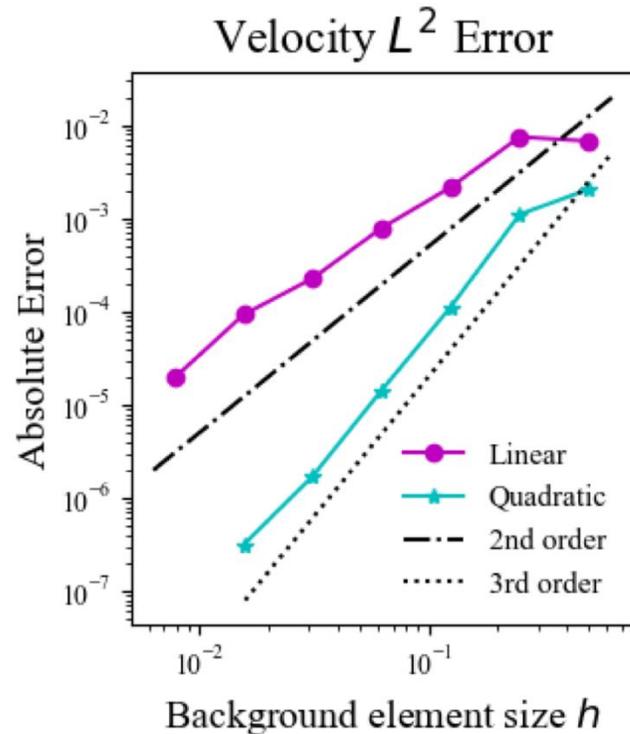


Image-Based Analysis for Composite Materials

Linear elastic analysis of alumina particles embedded in epoxy from Micro-CT image

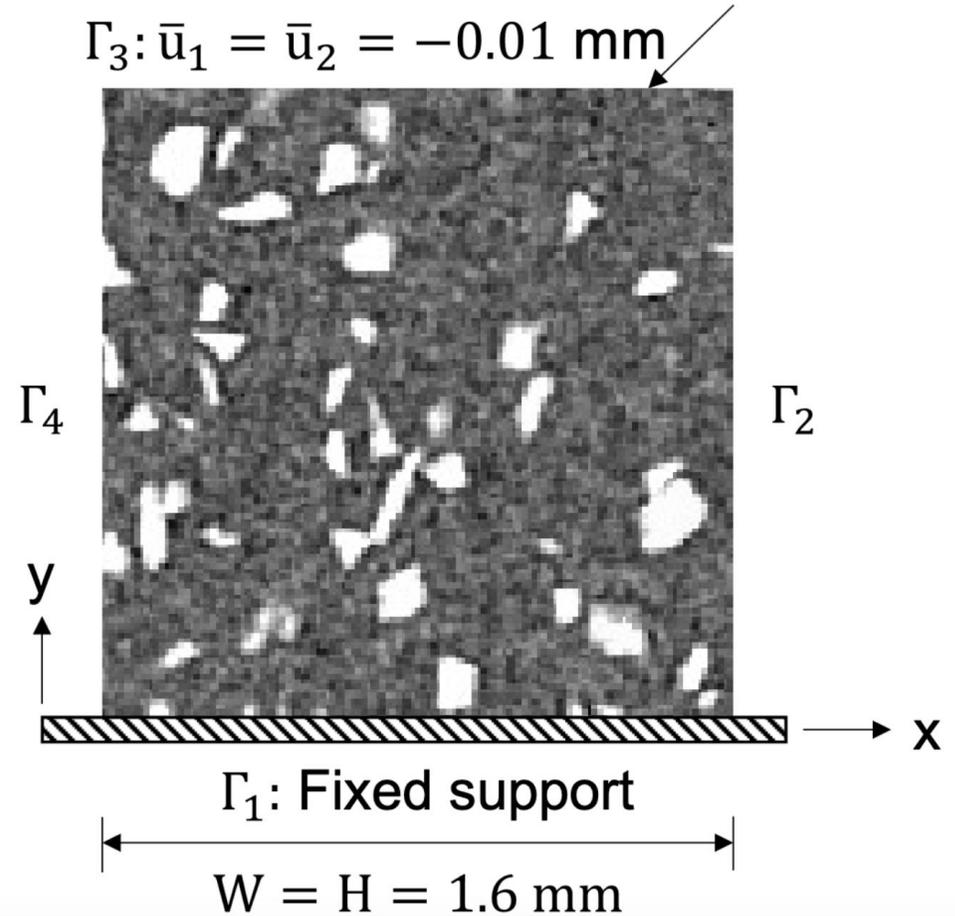
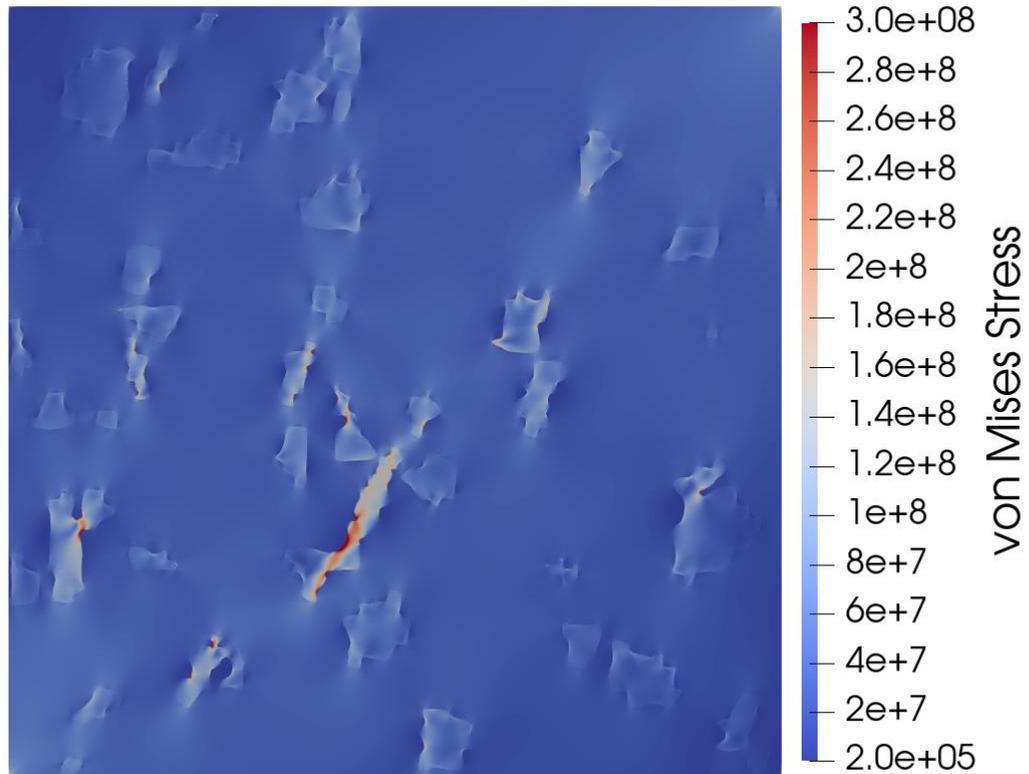
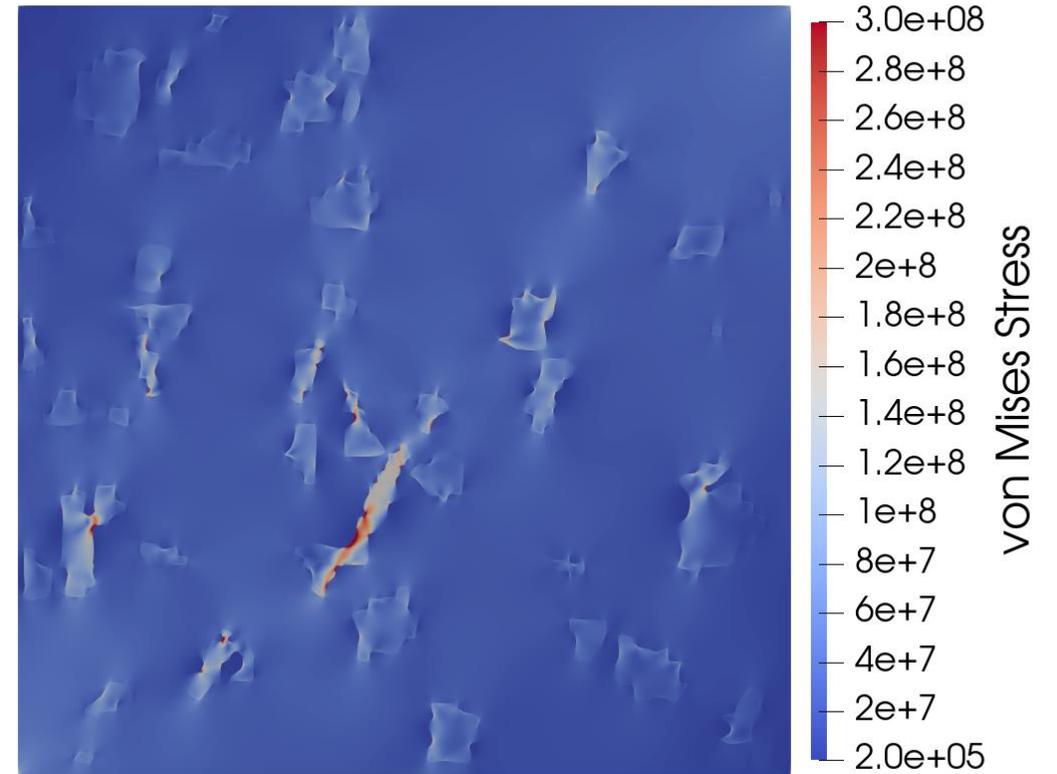


Image-Based Analysis for Composite Materials

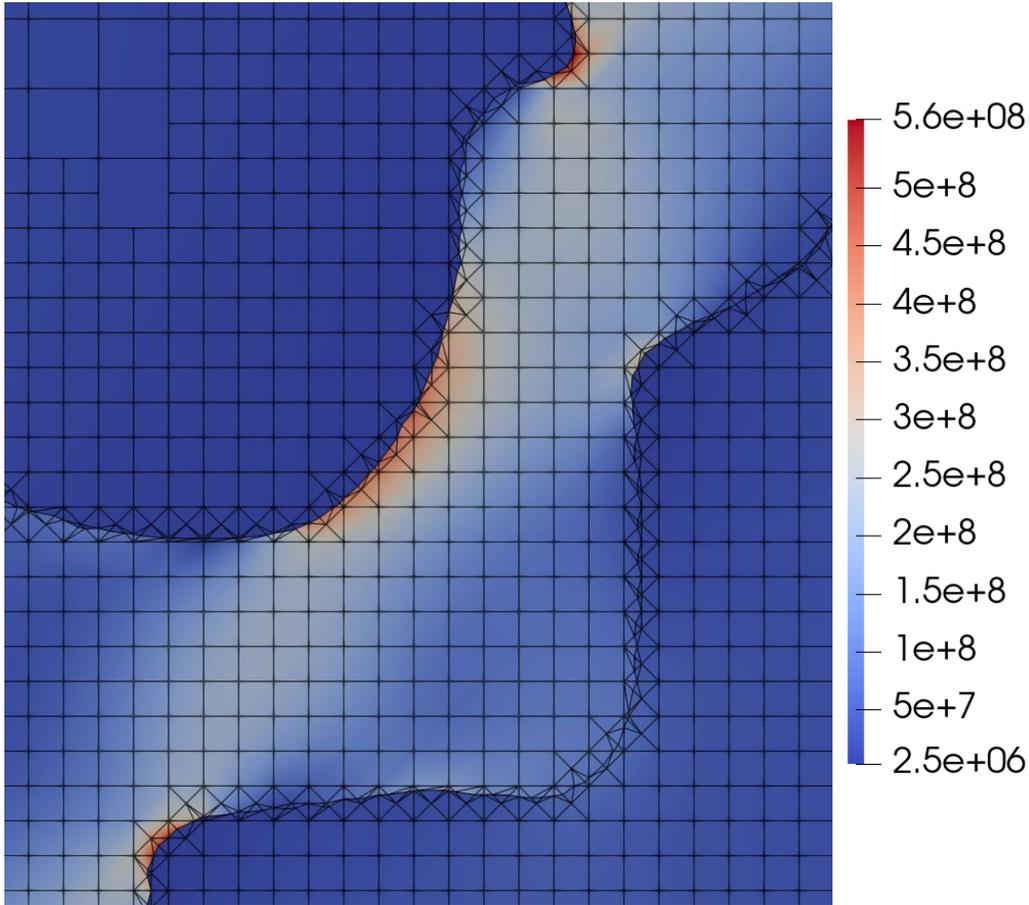


Immersed FEA

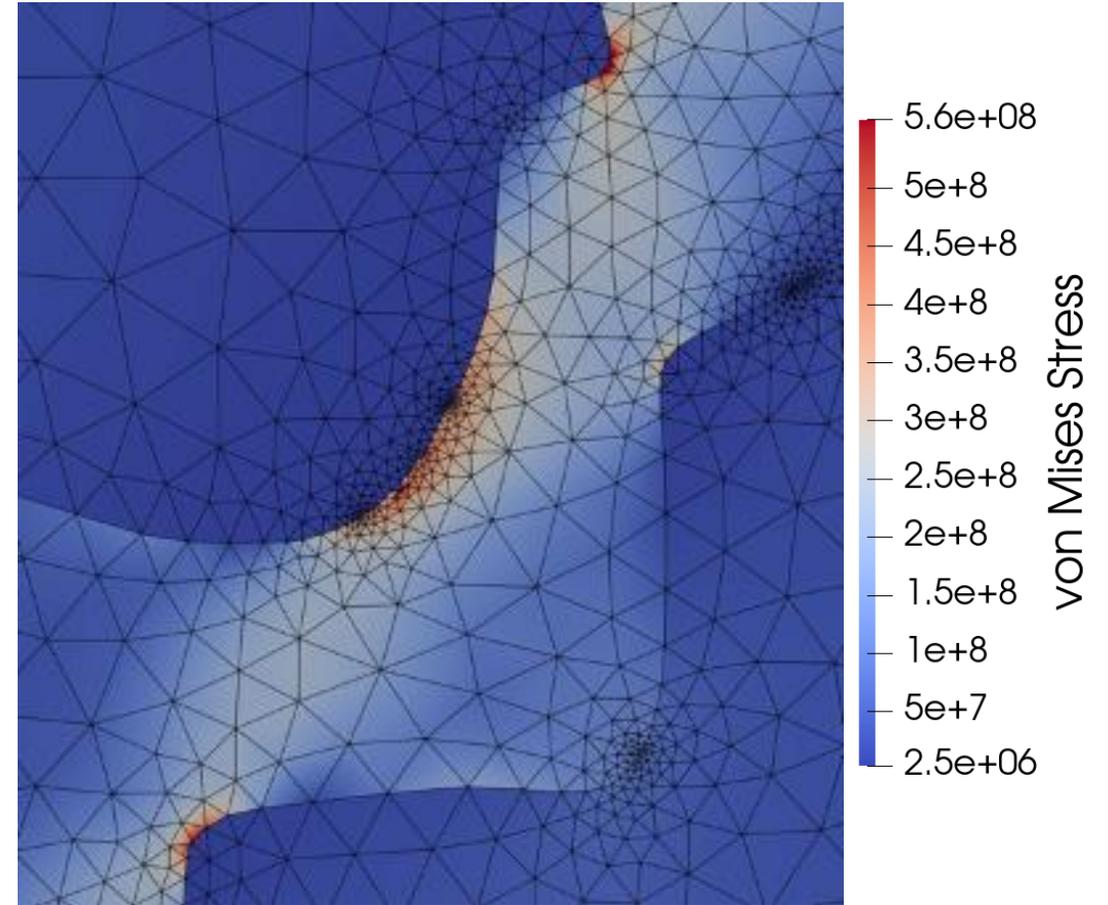


Body-Fitted FEA

Image-Based Analysis for Composite Materials



Immersed FEA



Body-Fitted FEA

Application to Thermo-Elasticity: Heating of Plate with Inclusion

Subdomain A:

$$E = 1.0$$

$$\nu = 0.3$$

$$\alpha = 1.0 \times 10^{-5}$$

Subdomain B:

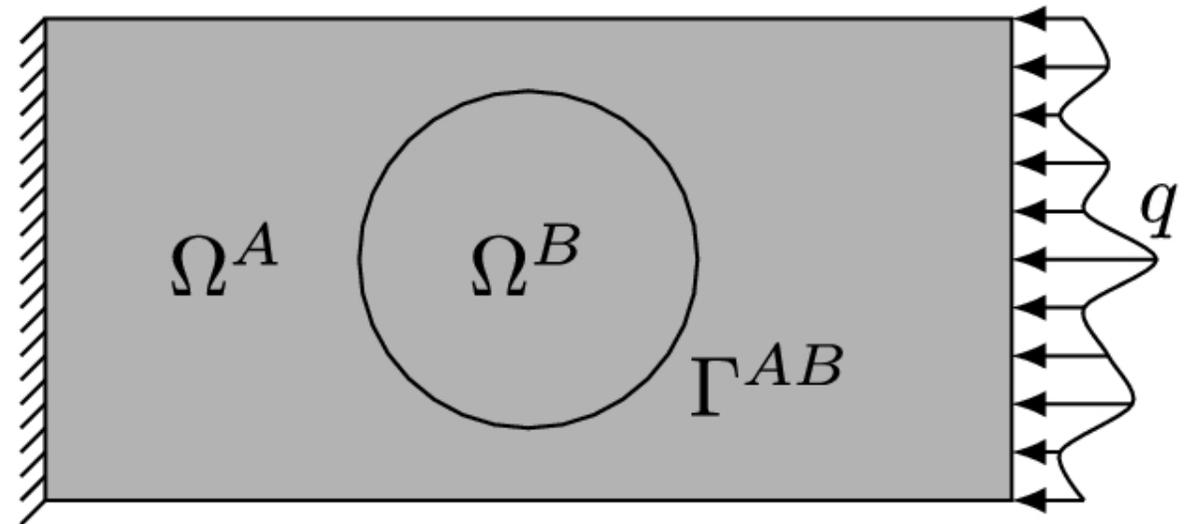
$$E = 1.0$$

$$\nu = 0.3$$

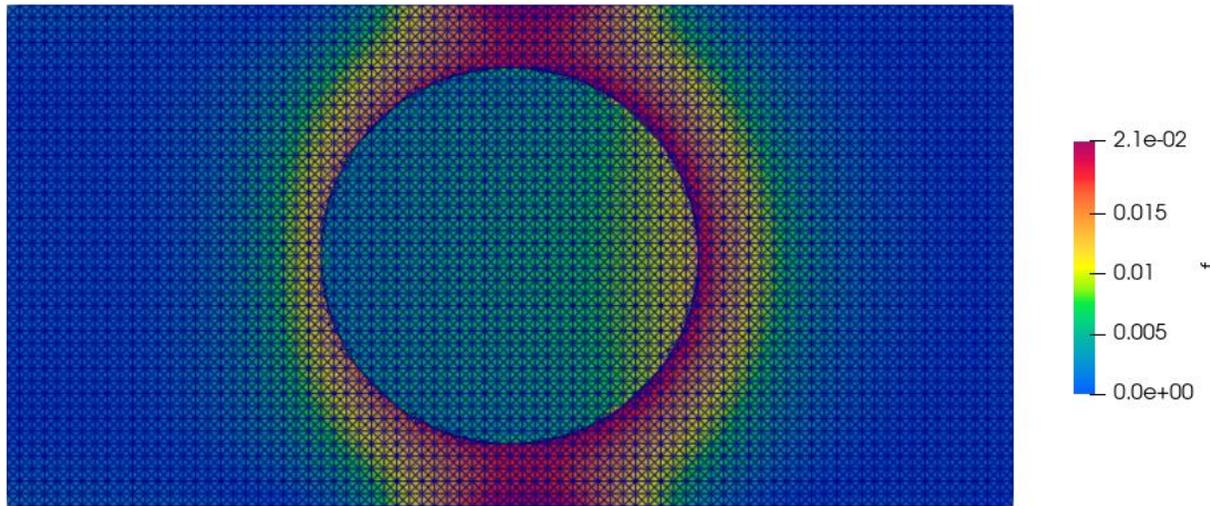
$$\alpha = 10.0 \times 10^{-5}$$

$$\mathbf{u} = \mathbf{0}$$

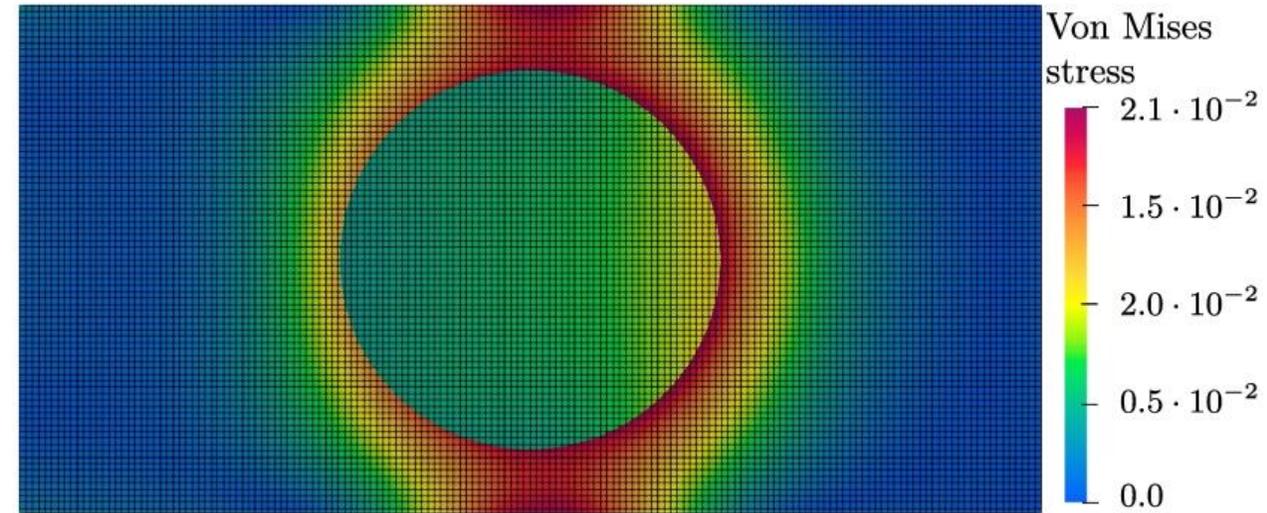
$$T = 0$$



Application to Thermo-Elasticity: Heating of Plate with Inclusion

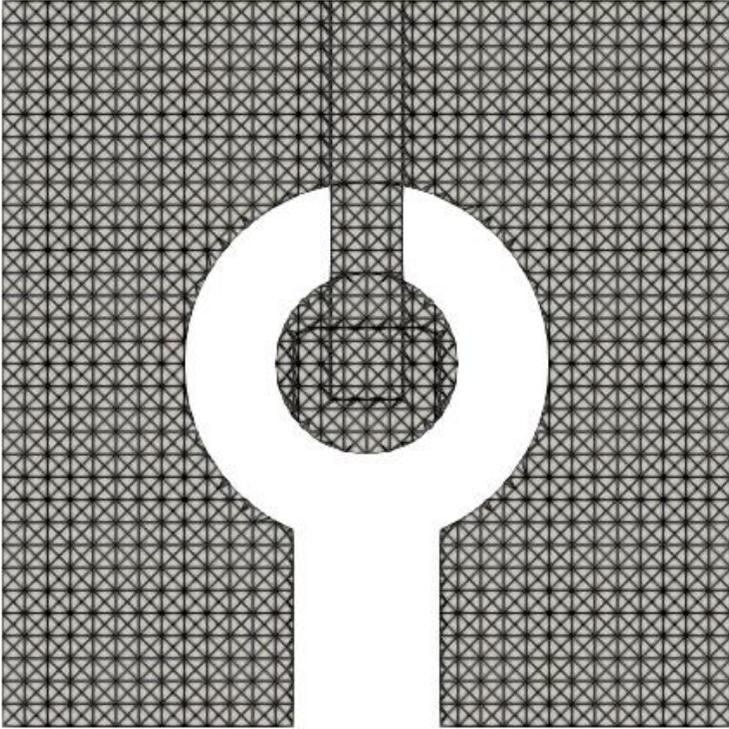


Interpolation-Based Immersed
Isogeometric Analysis $k_1 = k_1 = 2$

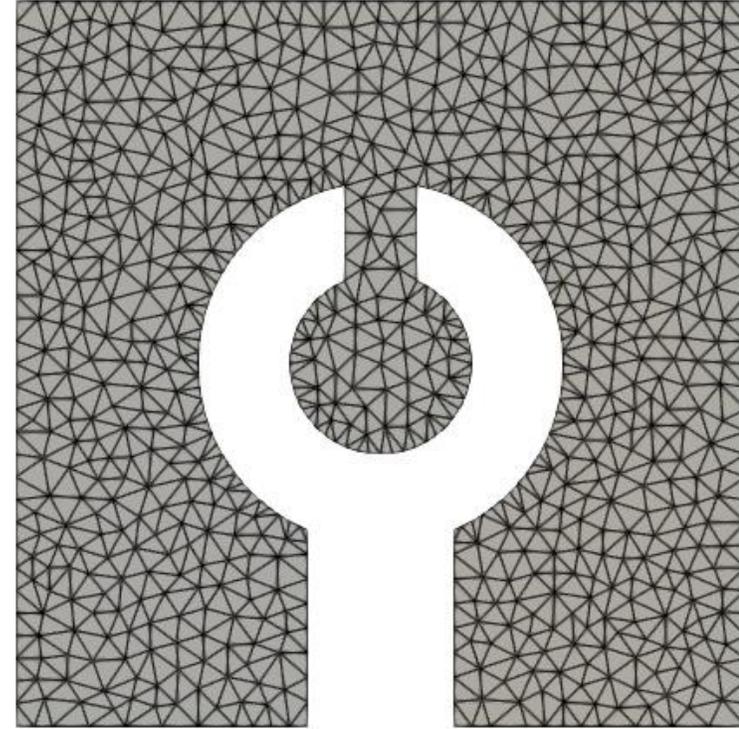


Quadrature-Based Immersed
Isogeometric Analysis $k_1 = k_1 = 2$

Interpolation-Based Trimmed Isogeometric Shell Analysis



Background-fitted foreground mesh

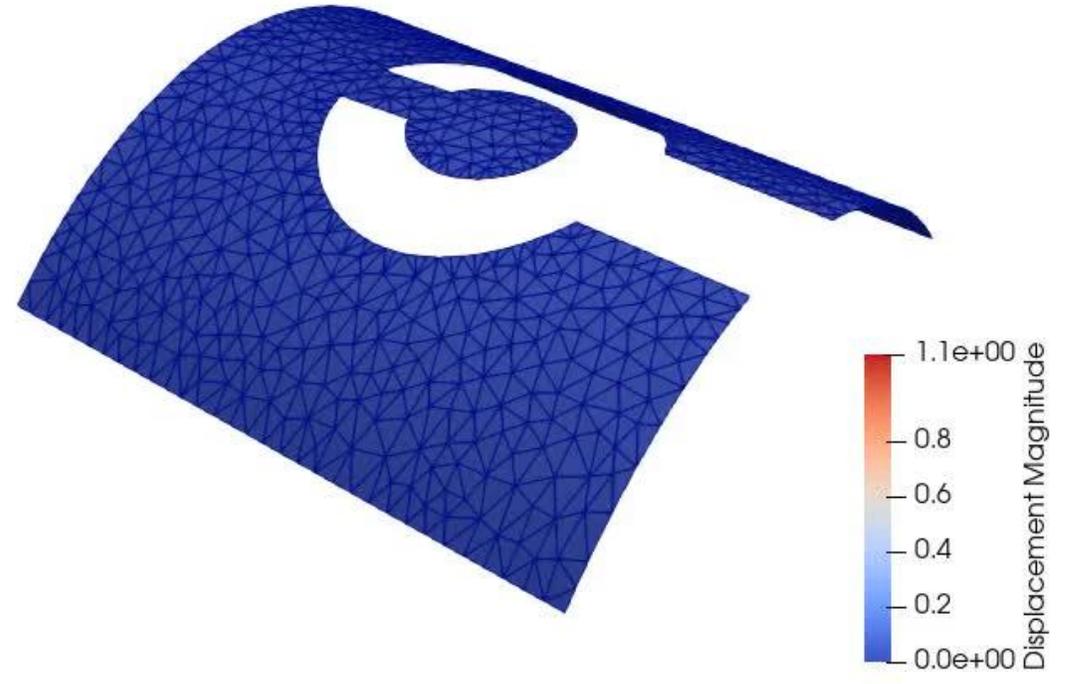


Background-unfitted foreground mesh

Interpolation-Based Trimmed Isogeometric Shell Analysis

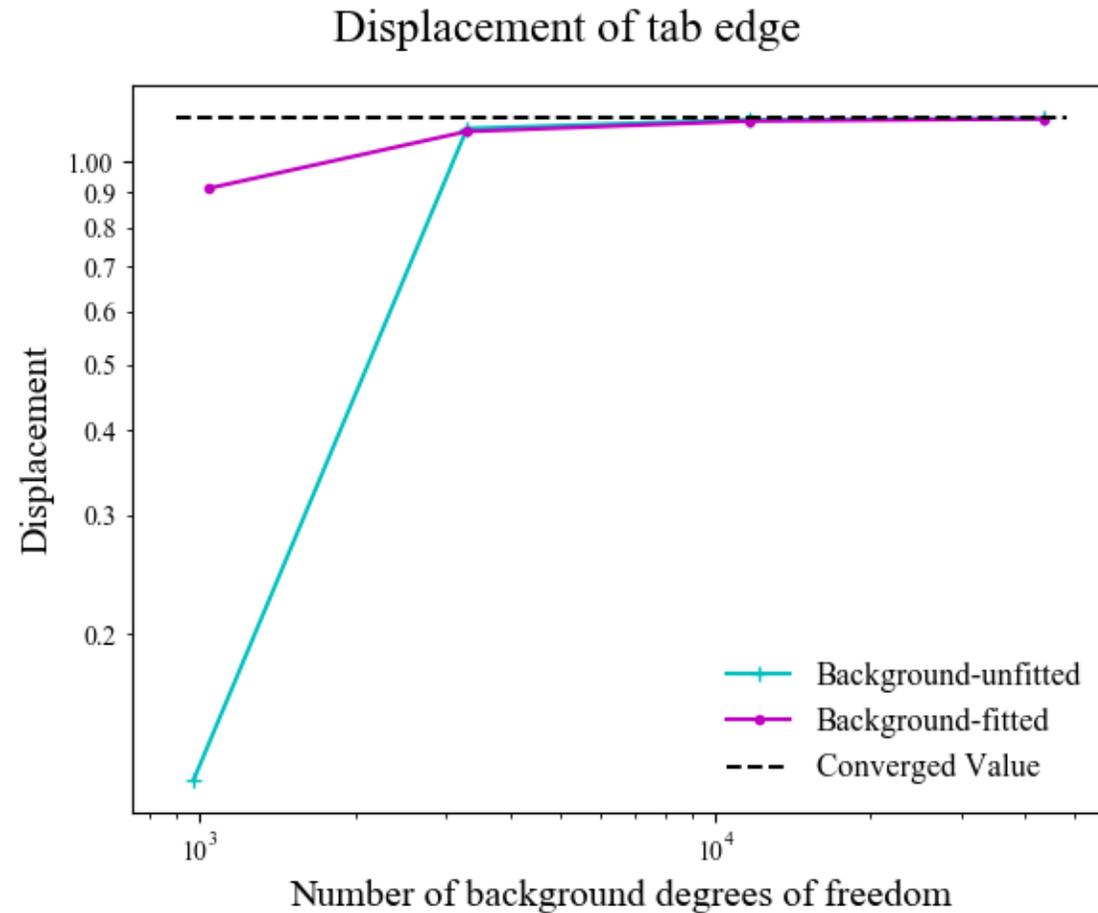


Background-fitted foreground mesh



Background-unfitted foreground mesh

Interpolation-Based Trimmed Isogeometric Shell Analysis

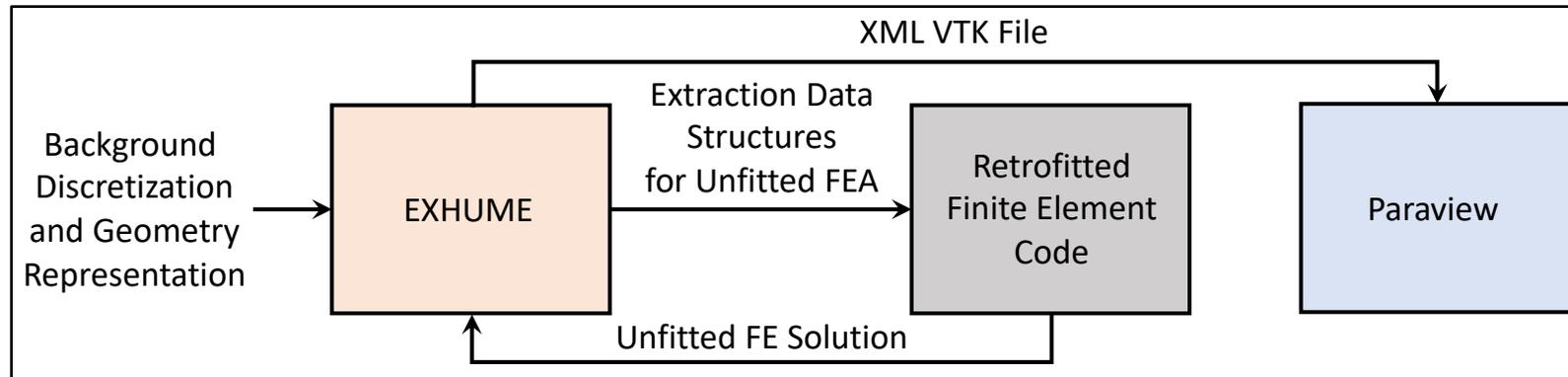


Part 3:

Transforming Classical Codes Into Immersed Codes with EXHUME

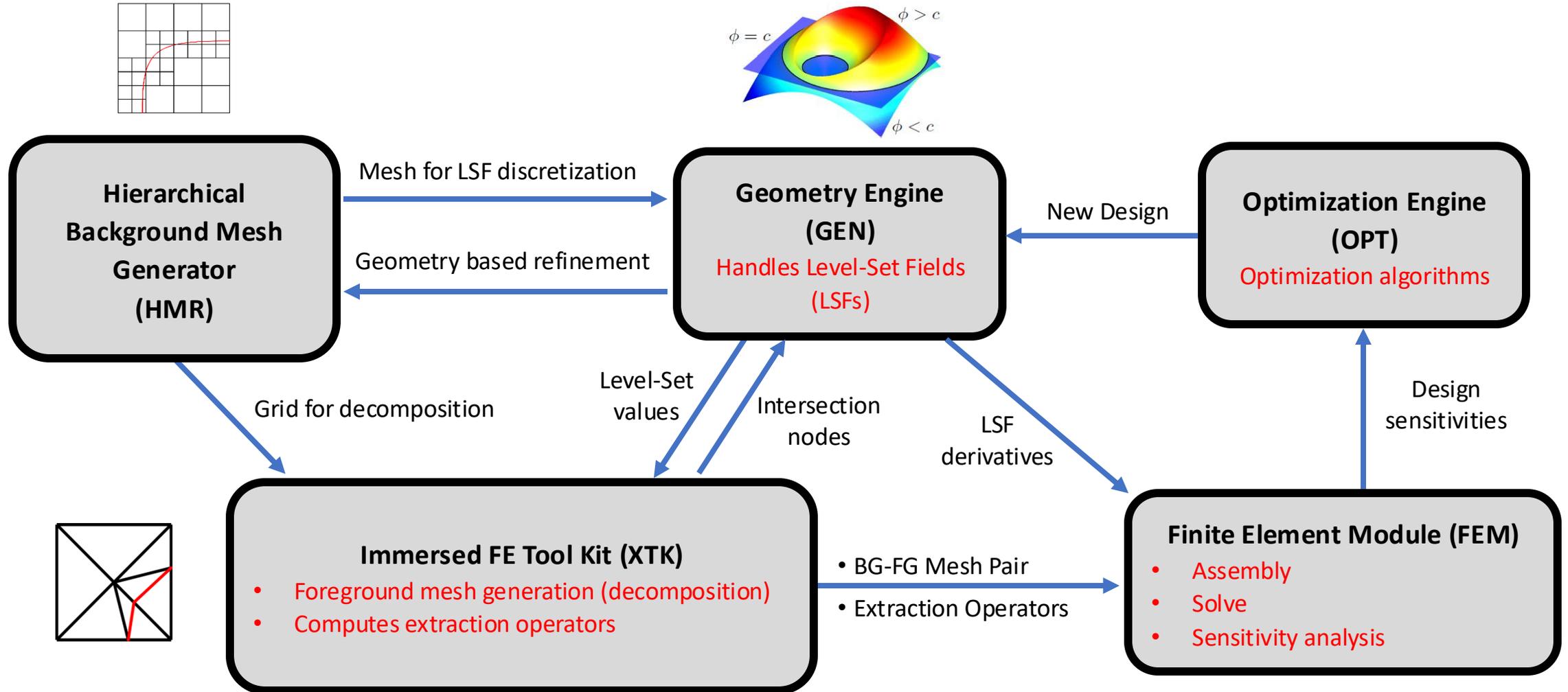
Retrofitting Classical Finite Element Codes for Interpolation-Based Immersed Analysis

Our software library [EXHUME](#) creates foreground meshes, extraction operators, and connectivity arrays outside of the confines of any particular finite element code:

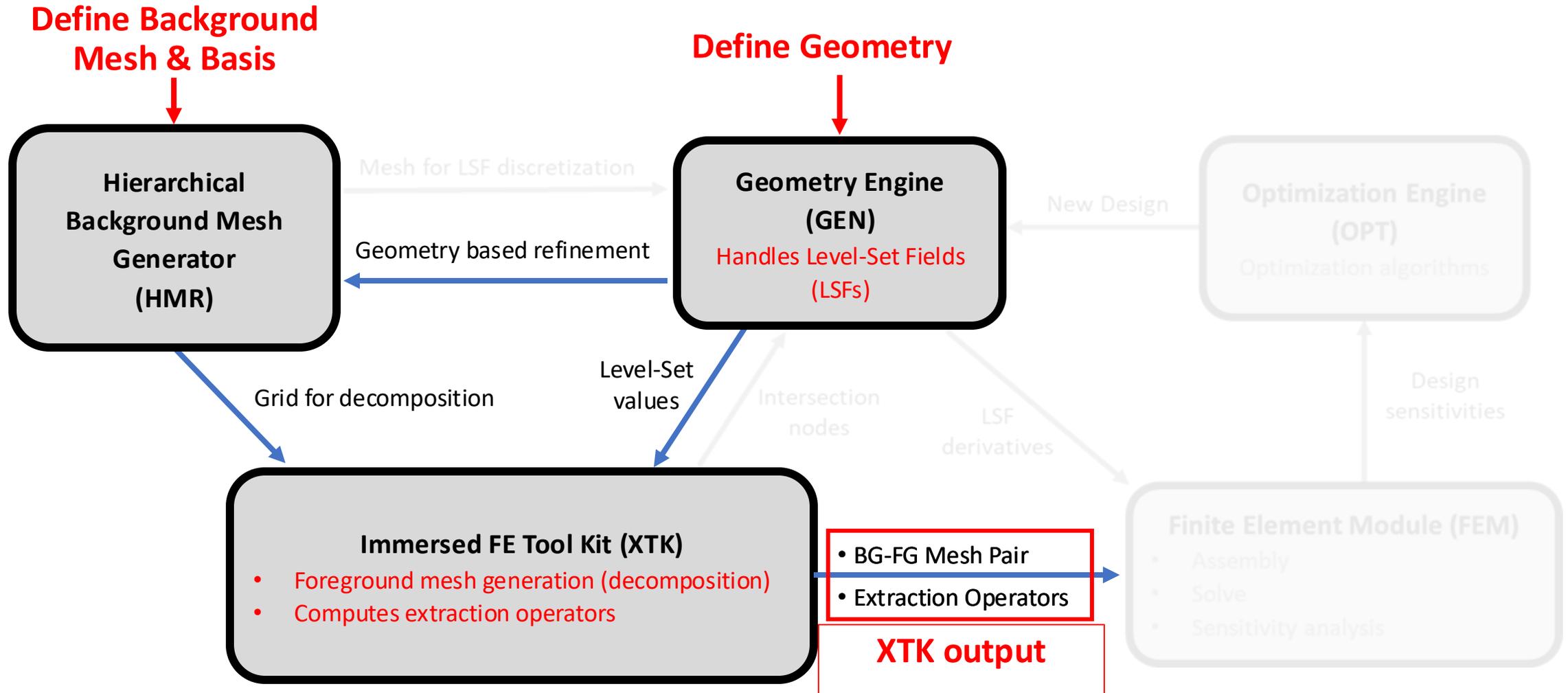


As demonstrated later, we have leveraged these extraction data structures to transform the popular open-source classical finite element code [FEniCS](#) into an interpolation-based immersed finite element code.

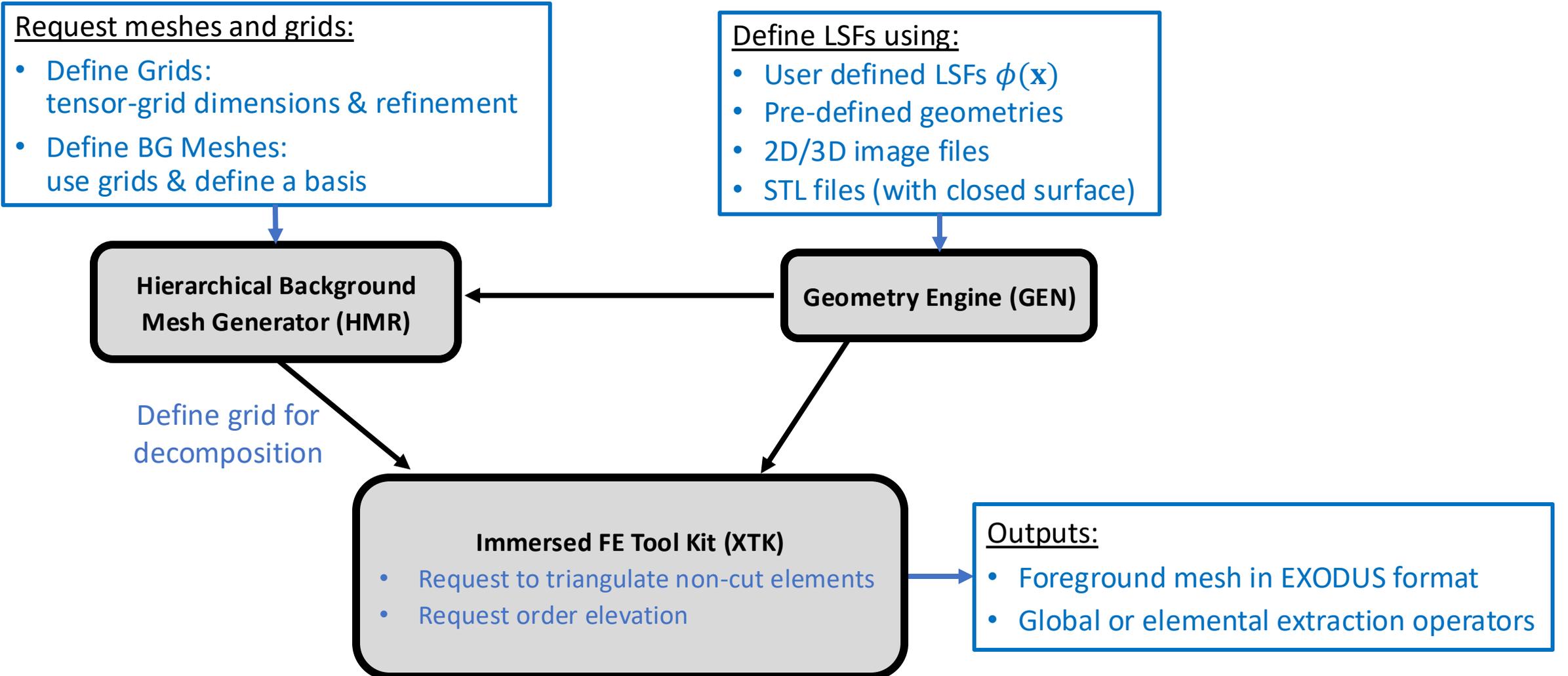
The MORIS Software Library for XFEM-Based Level Set Topology Optimization



The MORIS Software Library for XFEM-Based Level Set Topology Optimization



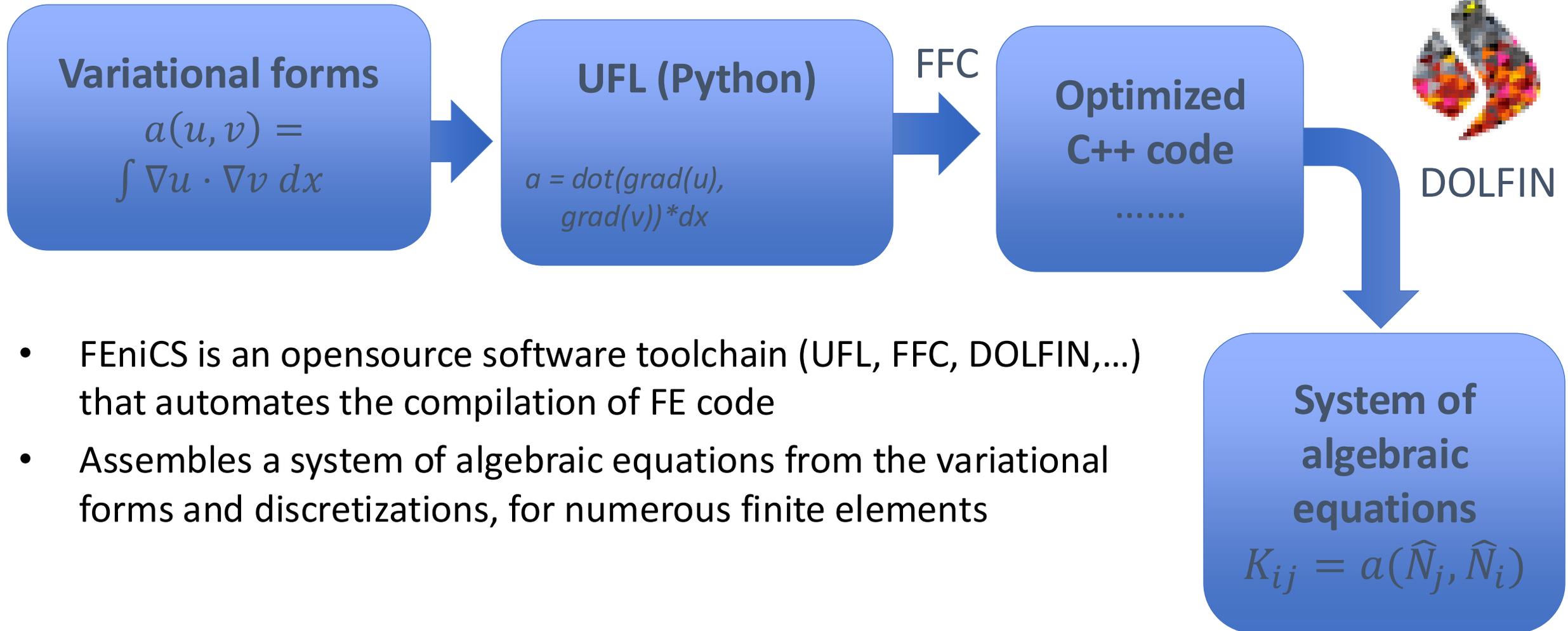
The EXHUME Software Library



Part 4:

Enabling Interpolation-Based Immersed FEA in FEniCS

Leveraging Code Generation: The FEniCS Project



- FEniCS is an opensource software toolchain (UFL, FFC, DOLFIN,...) that automates the compilation of FE code
- Assembles a system of algebraic equations from the variational forms and discretizations, for numerous finite elements

Interpolation-Based Immersed Finite Element Analysis Workflow

Generate foreground boundary-fitted mesh, and its extraction operator

$$M_{ij} = N_i(\mathbf{x}_j)$$



Assemble $A_{ij} = a(\phi_j, \phi_i)$ and $B_i = L(\phi_i)$ using foreground basis ϕ_i

Compute $\mathbf{K} = \mathbf{M}^T \mathbf{A} \mathbf{M}$ and $\mathbf{F} = \mathbf{M}^T \mathbf{B}$

Solve $\mathbf{K} \mathbf{d} = \mathbf{F}$

Project solution onto foreground basis for visualization and analysis:
 $\mathbf{u} = \mathbf{M}^T \mathbf{d}$

FEniCS: Solving the Poisson Problem with Classical FEA

Load mesh and
define subdomains

```
from dolfin import *

#load mesh, and define geometry subdomains
mesh_f = Mesh()
file = XDMFFile(mesh_f.mpi_comm(),'mesh.xdmf')
file.read(mesh_f)
sub_domains=MeshFunction('size_t',mesh_f,mesh_f.geometry().dim())
file.read(sub_domains,'material')
outside_ID = 1; block_ID = 2; surf_ID = 3
sub_domains_surf = MeshFunction("size_t",mesh_f,mesh_f.geometry().dim()-1)
> for facet in facets(mesh_f):--
dx_custom = Measure('dx', subdomain_data=sub_domains,subdomain_id=block_ID, metadata={'quadrature_degree': 2*k})
ds_custom = Measure('dS', subdomain_data=sub_domains_surf,subdomain_id=surf_ID, metadata={'quadrature_degree': 2*k})
```

Define classic FE
function space

```
#Define a foreground function space on the mesh, with continuous Galerkin elements, with polynomial order k = 2
k = 2
V_f = FunctionSpace(mesh_f, 'CG', k)
u_f = Function(V_f)
v_f = TestFunction(V_f)
int_constant = Constant(0.0)*v_f*dx(domain=mesh_f, subdomain_data=sub_domains)
```

Define variational
problem

```
# define the exact solution, to be used with the method of manufactured solutions
x = SpatialCoordinate(mesh)
u_ex = sin(x[0])*cos(x[1])
f = -div(grad(u_ex))
a = inner(grad(u_f),grad(v_f))*dx_custom
L = inner(f,v_f)*dx_custom
```

FEniCS: Solving the Poisson Problem with Classical FEA

Enforce boundary conditions

```
#solve with classic FE  
  
# strongly enforce boundary conditions  
def boundary(x,on_boundary):  
    | return on_boundary  
bc = DirichletBC(V_f, u_ex, sub_domains_surf, surf_ID)
```

Linear solve

```
#Compute the solution on the foreground mesh  
u = Function(V_f)  
solve(a==L, u, bc)
```

FEniCS: Solving the Poisson Problem with Interpolation-Based Immersed FEA

Load EXHUME module

Enforce boundary conditions with Nitsche's method

Transform matrix system

Linear solve

```
# solve using the interpolation-based immersed boundary method
# import EXHUME module
from EXHUME.common import * ;
from EXHUME.la_utils import * ;

# weakly enforce boundary conditions using Nitsche's method
n = FacetNormal(mesh_f)
h_E = CellDiameter(mesh_f)("+")
beta = Constant(10) # user specified penalty parameter
nitsche_form = -inner(dot(grad(u_f("+")), n("+")), v_f("+"))*ds_custom + int_constant
nitsche_consistency = inner(u_ex("+")-u_f("+"), dot(grad(v_f("+")), n("+")))*ds_custom + int_constant
nitsche_penalty = beta*h_E**(-1)*inner(u_f("+")-u_ex("+"), v_f("+"))*ds_custom + int_constant

# define the residual and it's jacobian
res = a - L + nitsche_form + nitsche_consistency + nitsche_penalty
J_f = derivative(res, u_f)
res_f_P = as_backend_type(assemble(res)).vec() # convert to PETSc vector
J_f_P = as_backend_type(assemble(J_f)).mat() # convert to PETSc matrix

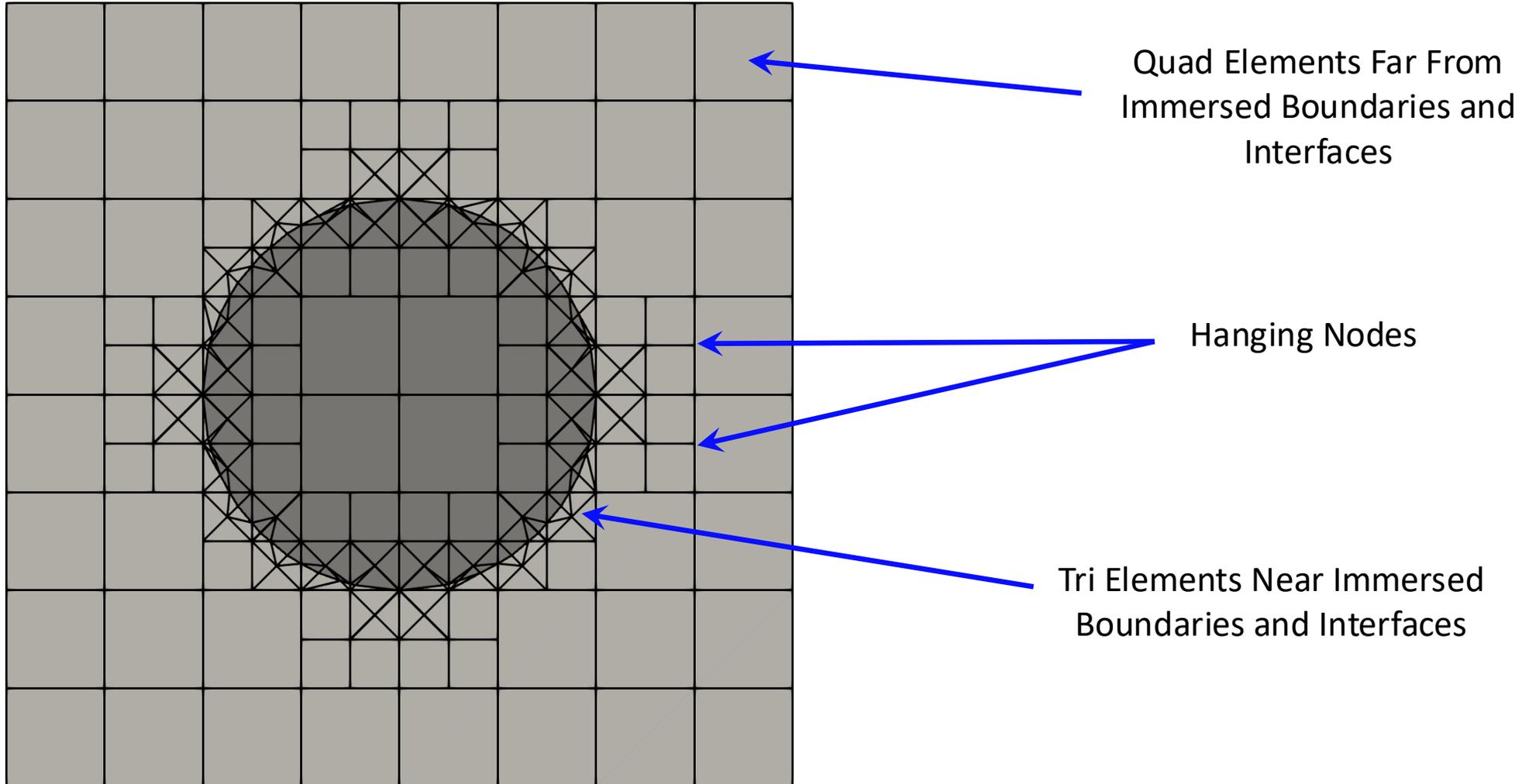
# Read in Extraction Operator, and interpolate |
local_size = v2p(assemble(res)).getLocalSize() #determine local matrix size
M = readFromCSV_Notebook(['ExOp_Cons.csv'],V_f,mesh_f,local_size,nodeFileNames='cell_nodes.csv',k=k);
M.assemble()
J_b = AT_R_A(M,J_f_P)
res_b = AT_x(M,res_f_P)
u_b = J_b.createVecLeft()
solveKSP(J_b,-res_b,u_b, method='gmres', PC='jacobi',monitor=False)

# project onto the foreground basis for analysis
u_f_p = as_backend_type(u_f.vector()).vec()
M.mult(u_b,u_f_p)
updateU(u_f)
```

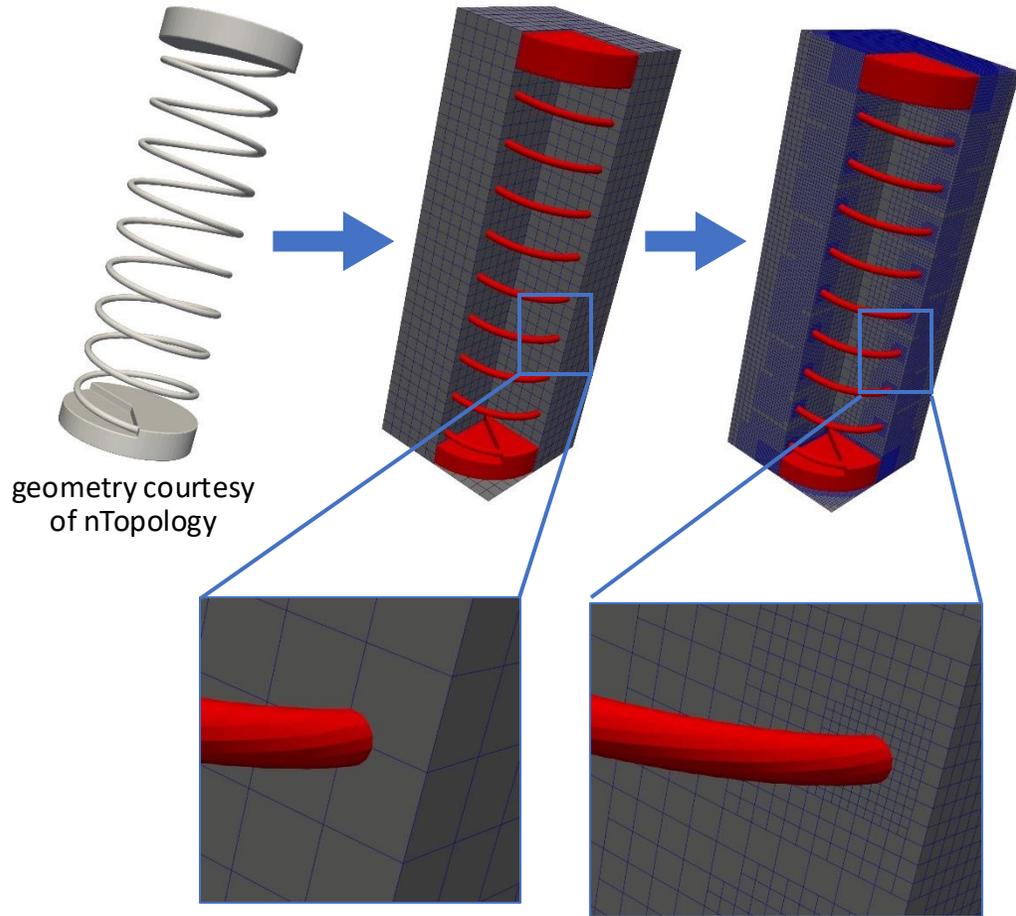
Part 5:

Current Status and Future Plans

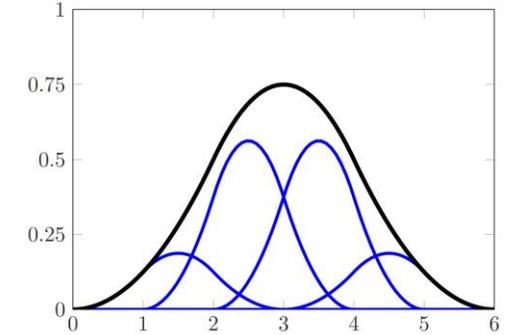
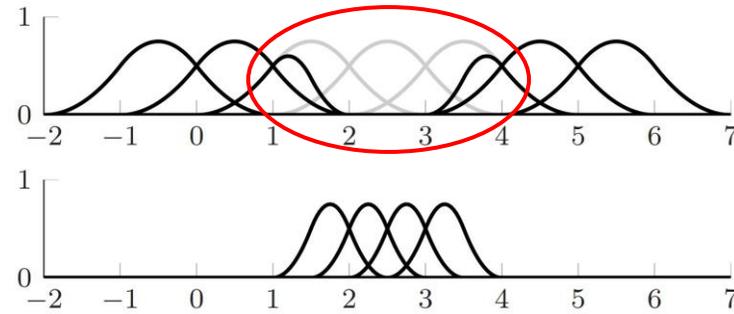
Capability #1: Support for Locally Refined Mixed Foreground Meshes of Tris/Quads (in 2D) and Tets/Hexes (in 3D) with Hanging Nodes



Capability #2: Support for Locally Refined Background Discretizations of Hierarchical B-splines



Hierarchical basis enables refinement

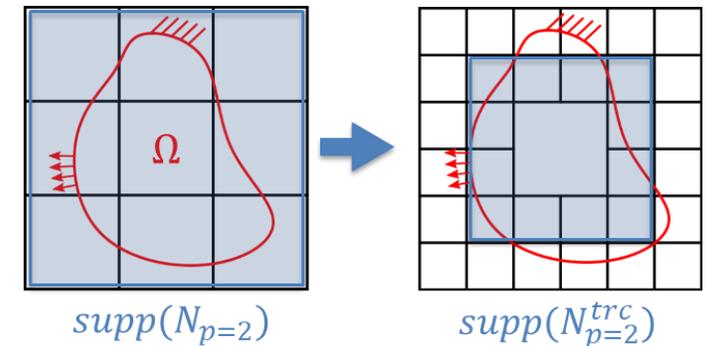


Basis function is sum of scaled and translated versions of itself

- Repeated refinement where needed

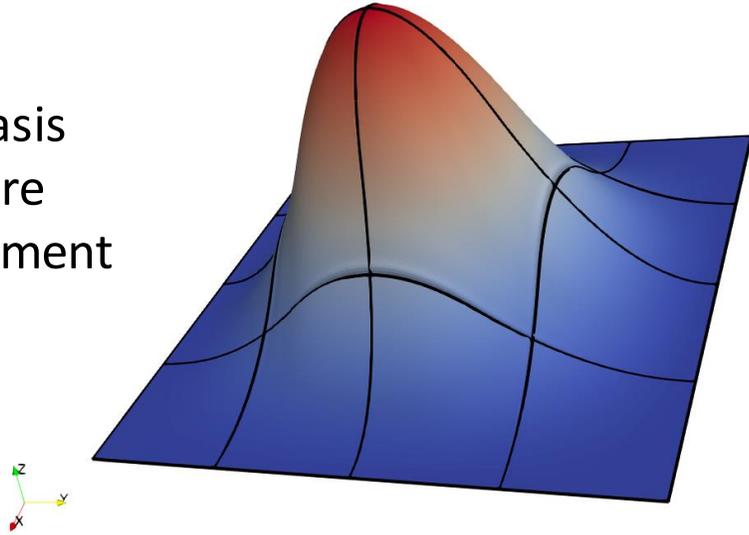
Truncation leads to:

- Reduced support size
- Retain partition of unity

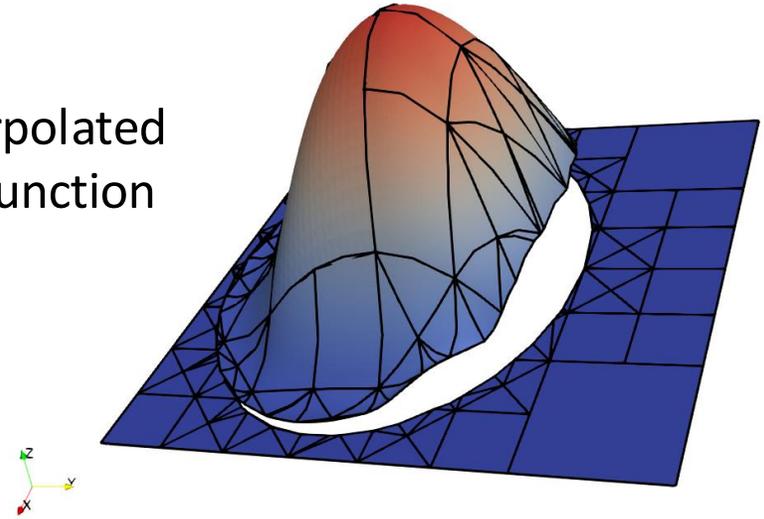


Capability #3: Support for Enriched Background Discretizations for Multi-Material Problems

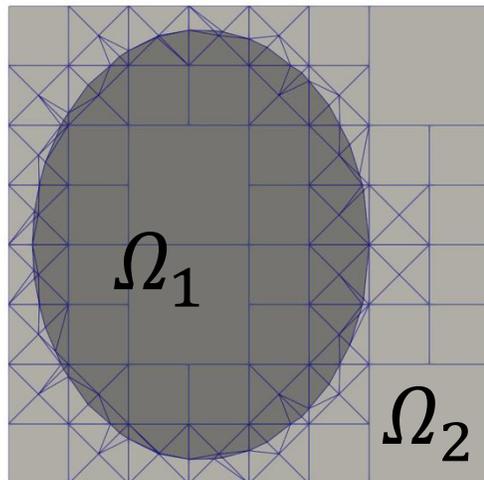
Background basis function before Heaviside enrichment



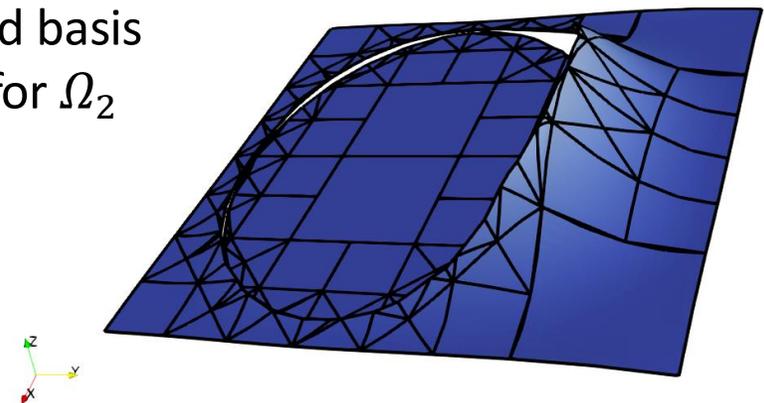
Enriched interpolated background function for Ω_1



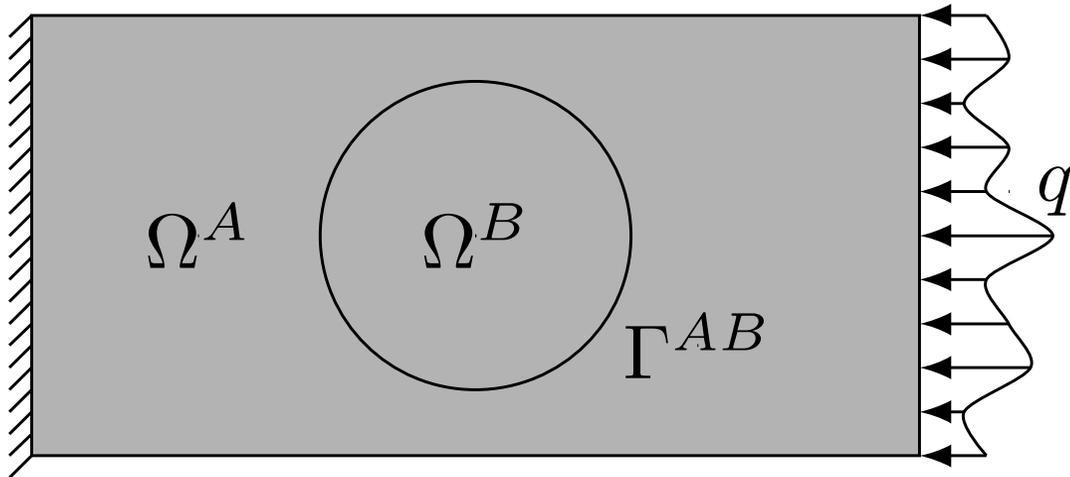
Foreground mesh with local refinement



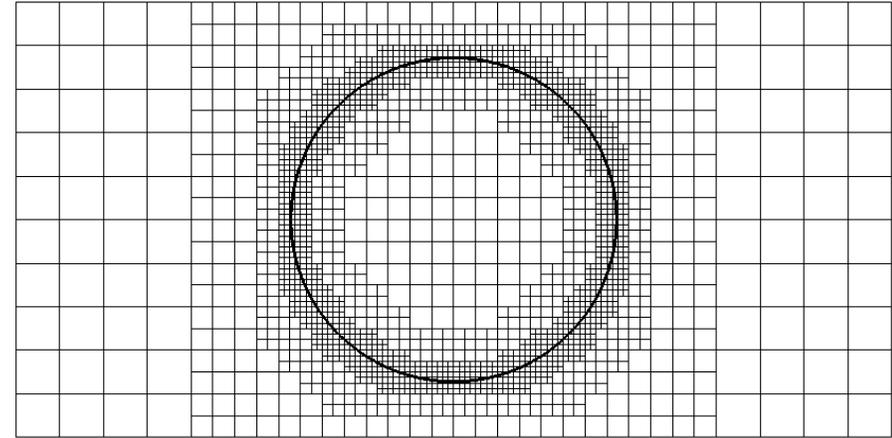
Enriched interpolated background basis function for Ω_2



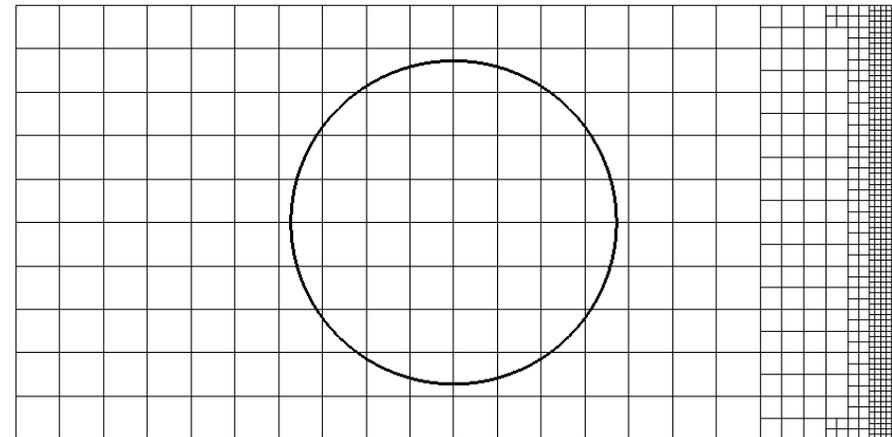
Capability #4: Support for Separate Background Discretizations for Multi-Physics Problems



Thermo-elastic multi-material problem
subject to a spatially varying heat load



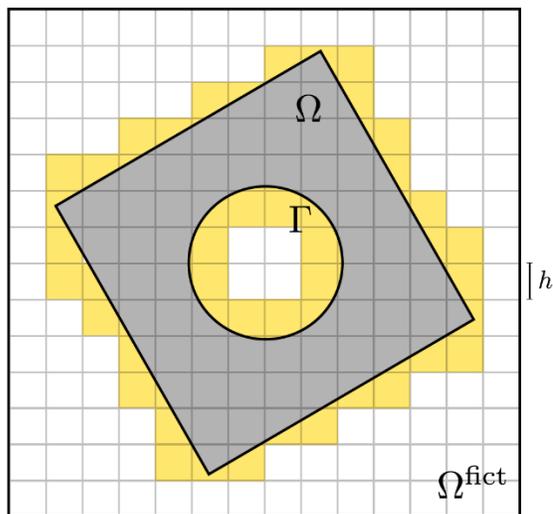
Background mesh for displacement field



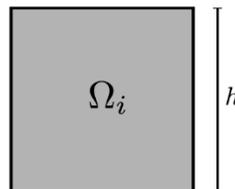
Background mesh for temperature field

Capability #5: Basis Stabilization in Presence of Small Cut Cells

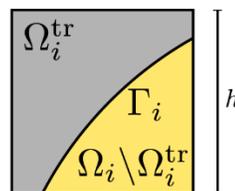
Issue: Stability and condition number deteriorate in the presence of small cut cells



Untrimmed cell

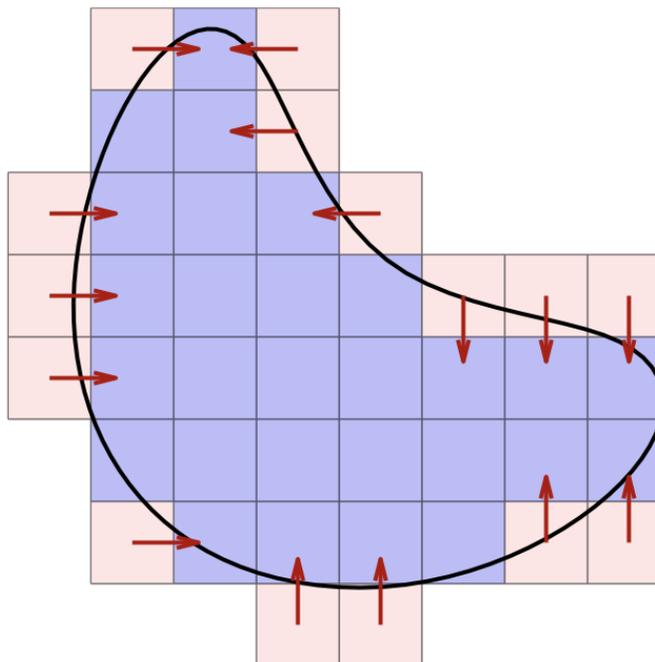


Trimmed cell



Solution: Remove basis functions with small support and modify remaining basis functions to maintain:

- (i) polynomial completeness
- (ii) partition of unity



Step 1: For each bad element, extend basis functions from neighboring good element

Step 2: Project back into original spline space

$$\kappa \sim \eta^{-\left(2p+1-\frac{2}{d}\right)} \quad \text{where} \quad \eta = \min_i \frac{|\Omega_i^{\text{tr}}|}{|\Omega_i|}$$

The end-user does not need to modify their analysis code or workflow to include stabilization – it only affects the extraction operators and connectivity!

Planned Capabilities

Support for [foreground meshes of curved integration elements](#) is currently being implemented.

Support for [Boundary Representation \(B-Rep\) geometric descriptions](#) is currently being implemented.

We are also equipping EXHUME with the capability to generate and output [cut-cell quadrature rules](#).

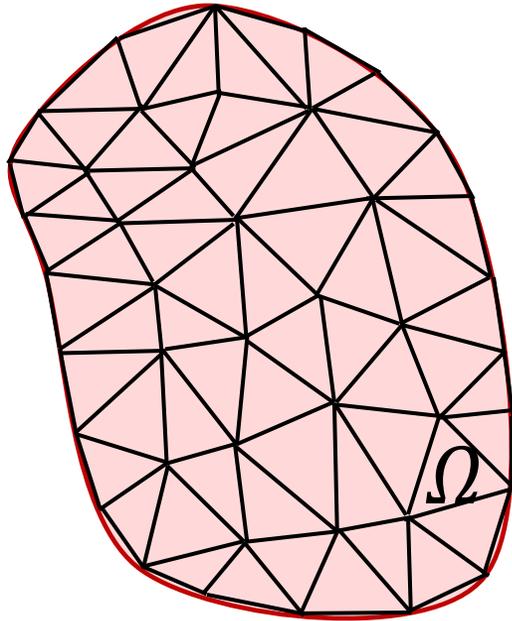
Part 6:

Can Interpolation Be Used To Enable Other Capabilities in FEniCS?



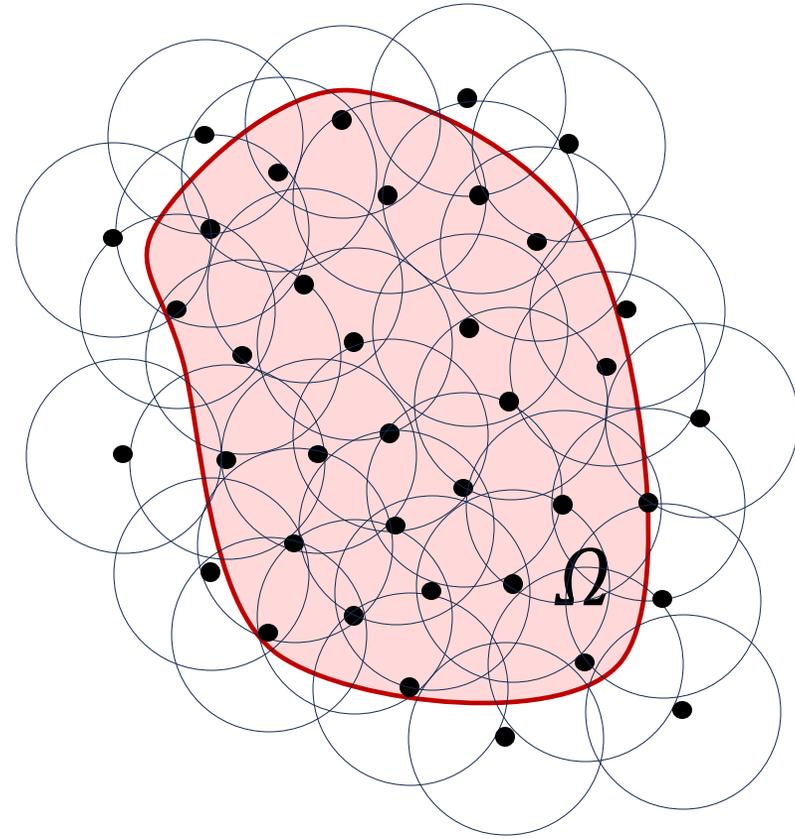
Jennifer Fromm

A (brief) introduction to meshfree methods



Classic Finite Element (FE):

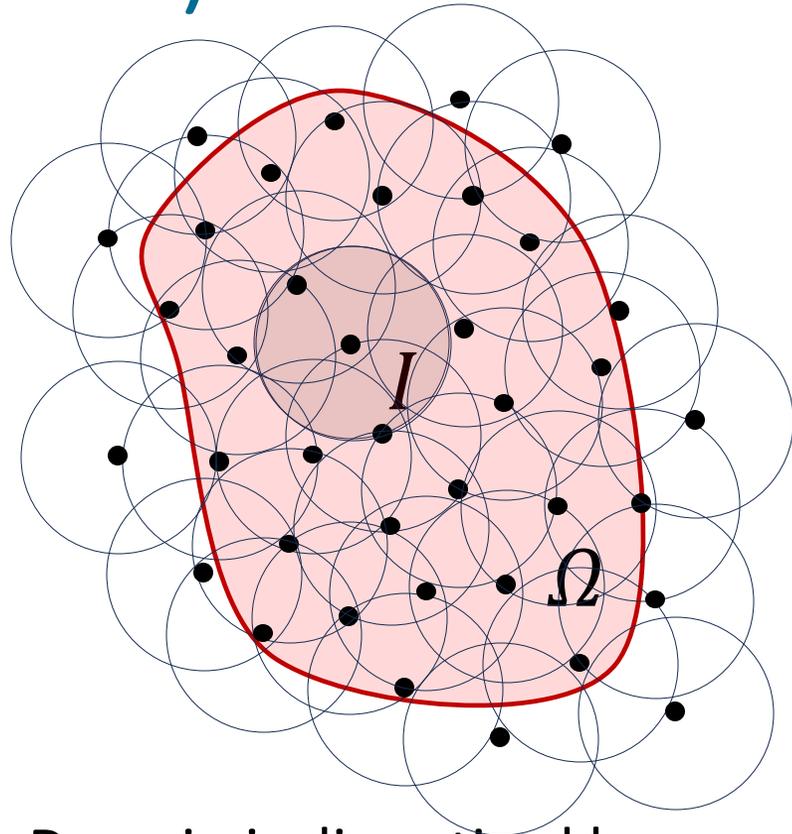
Domain is discretized by a boundary fitted mesh



Meshfree methods:

Domain is discretized by a point cloud

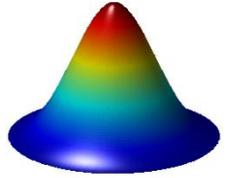
Meshfree methods: the reproducing kernel particle method (RKPM)



Domain is discretized by a point cloud

$$\Psi_I(\mathbf{x}) = C(\mathbf{x}; \mathbf{x} - \mathbf{x}_I) \phi_a(\mathbf{x} - \mathbf{x}_I)$$

Shape	Correction	Kernel
Function	Function	Function



Typically B-splines

$$C(\mathbf{x}; \mathbf{x} - \mathbf{x}_I) = \mathbf{H}^T(0) \mathbf{M}^{-1}(\mathbf{x}) \mathbf{H}(\mathbf{x} - \mathbf{x}_I)$$

Basis Vector:

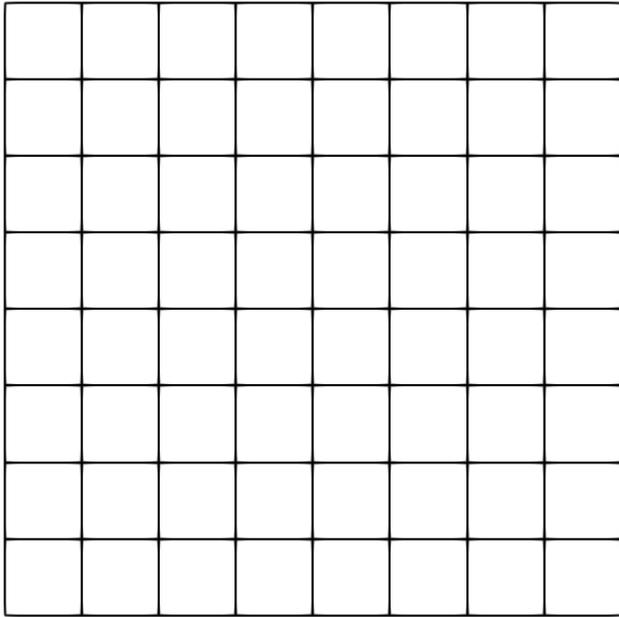
$$\mathbf{H}(\mathbf{x}) = [1, x, y, x^2, xy, y^2, \dots, xy^{n-1}, y^n]$$

Moment Matrix:

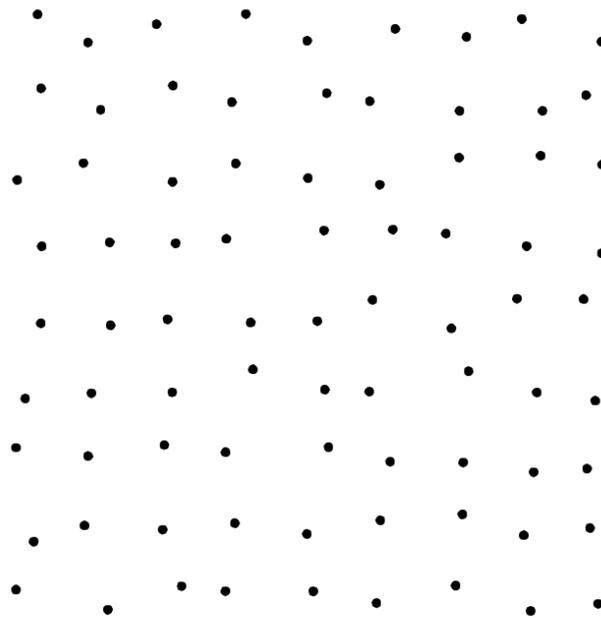
$$\mathbf{M}(\mathbf{x}) = \sum_I \mathbf{H}(\mathbf{x} - \mathbf{x}_I) \mathbf{H}^T(\mathbf{x} - \mathbf{x}_I) \phi_a(\mathbf{x} - \mathbf{x}_I)$$

Chen, J. S., Pan, C., Wu, C. T., and Liu, W. K., "Reproducing Kernel Particle Methods for Large Deformation Analysis of Nonlinear Structures," *Computer Methods in Applied Mechanics and Engineering*, Vol. 139, pp. 195-227, 1996.

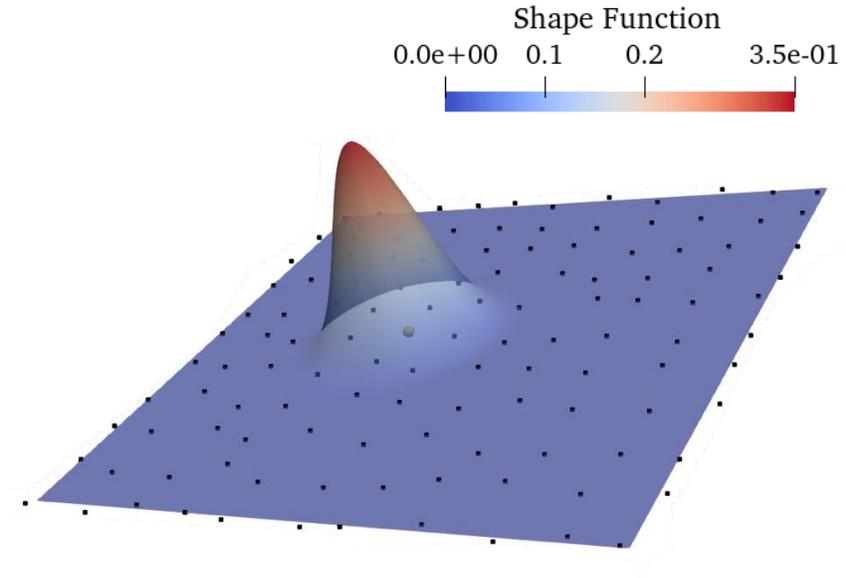
Interpolated-RKPM: introducing a foreground mesh



Foreground integration mesh, with Lagrange polynomial basis $\{N_i\}_{i=0}^v$



RKPM point cloud



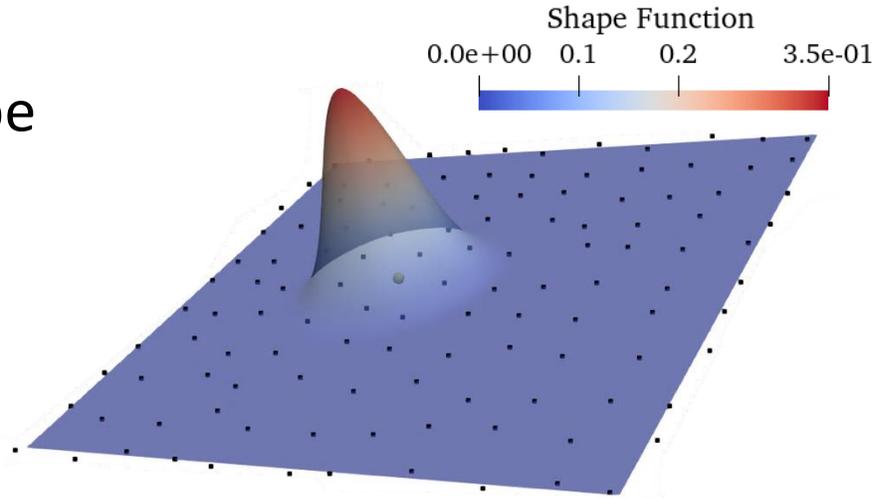
Linear RKPM shape function $\Psi_I(\mathbf{x})$

Each shape function can be interpolated: $\hat{\Psi}_I(\mathbf{x}) = \sum_{i=0}^v M_{Ij} N_j(\mathbf{x})$ With extraction operator $M_{Ij} = \Psi_I(\mathbf{x}_j)$

Int-RKPM shape functions: equal element size and polynomial order

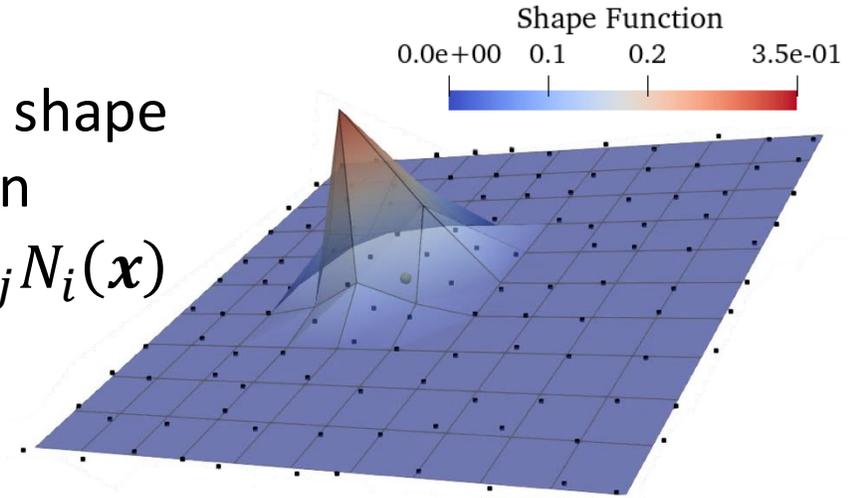
Linear shape function

$$\Psi_I(\mathbf{x})$$



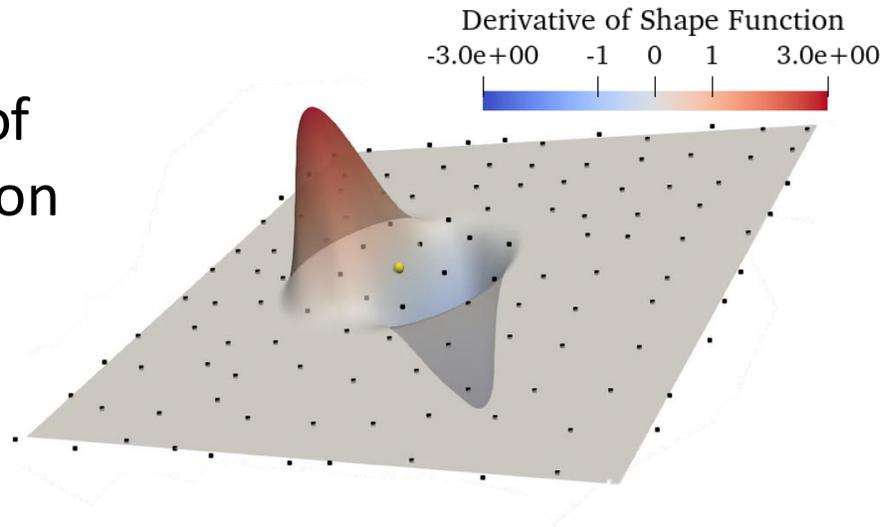
Interpolated shape function

$$\hat{\Psi}_I(\mathbf{x}) = \mathbf{M}_{Ij} N_i(\mathbf{x})$$



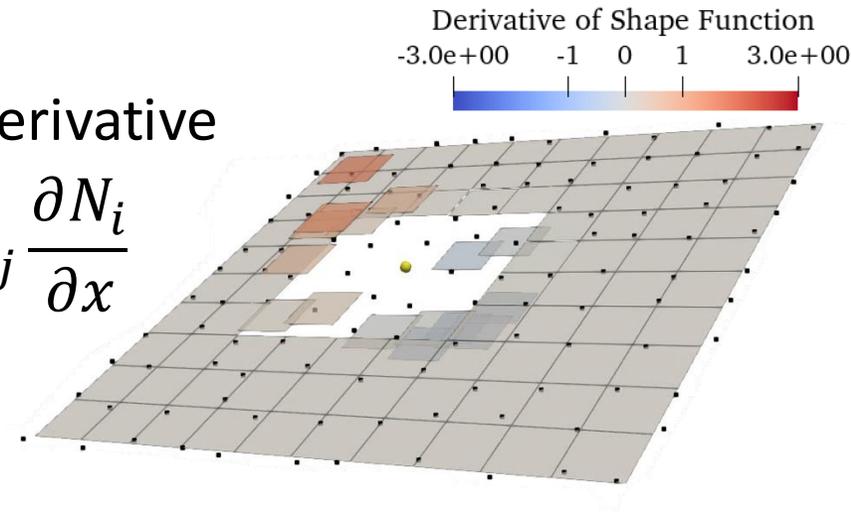
Derivative of shape function

$$\frac{\partial \Psi_I}{\partial x}$$



Interpolated derivative

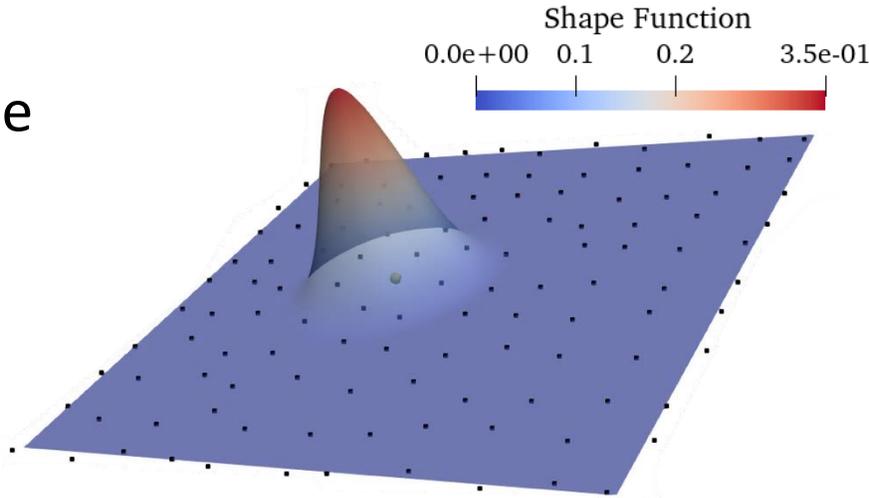
$$\frac{\partial \hat{\Psi}_I}{\partial x} = \mathbf{M}_{Ij} \frac{\partial N_i}{\partial x}$$



Int-RKPM shape functions: foreground h-refinement

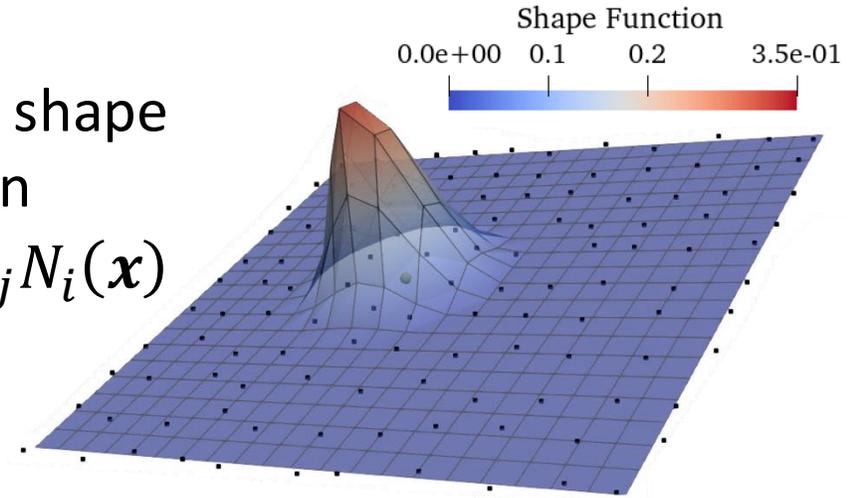
Linear shape function

$$\Psi_I(\mathbf{x})$$



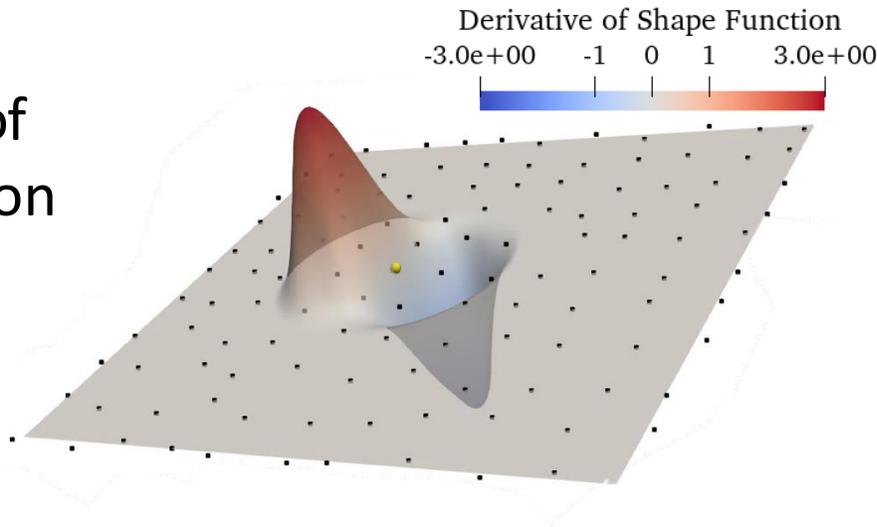
Interpolated shape function

$$\hat{\Psi}_I(\mathbf{x}) = \mathbf{M}_{Ij} N_i(\mathbf{x})$$



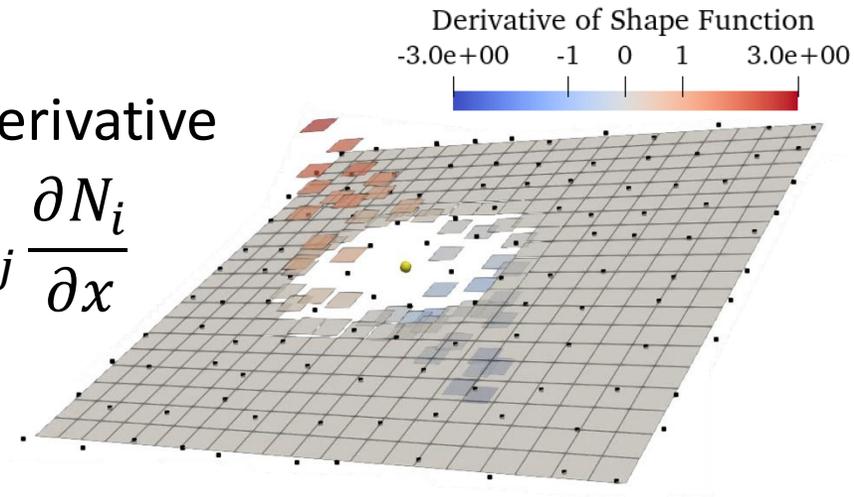
Derivative of shape function

$$\frac{\partial \Psi_I}{\partial x}$$



Interpolated derivative

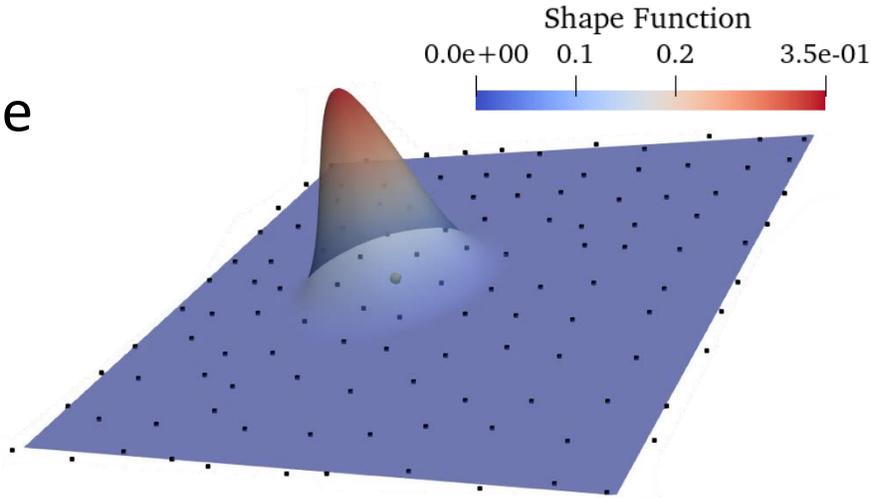
$$\frac{\partial \hat{\Psi}_I}{\partial x} = \mathbf{M}_{Ij} \frac{\partial N_i}{\partial x}$$



Int-RKPM shape functions: foreground p-refinement

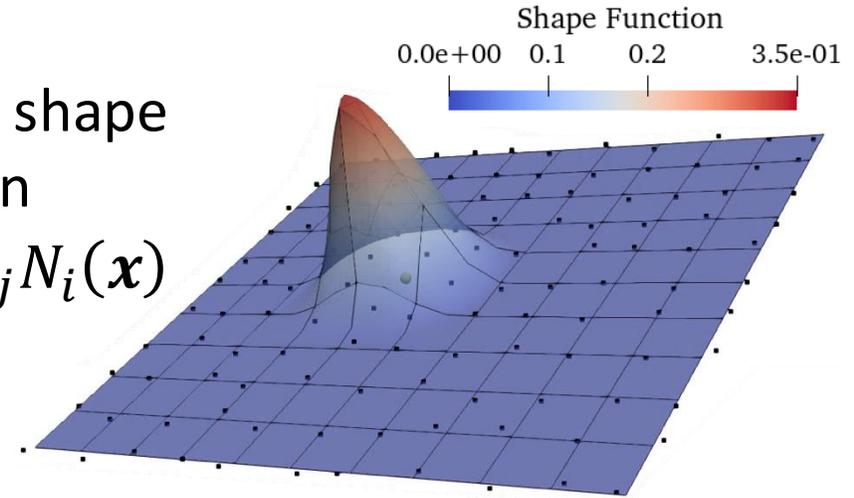
Linear shape function

$$\Psi_I(\mathbf{x})$$



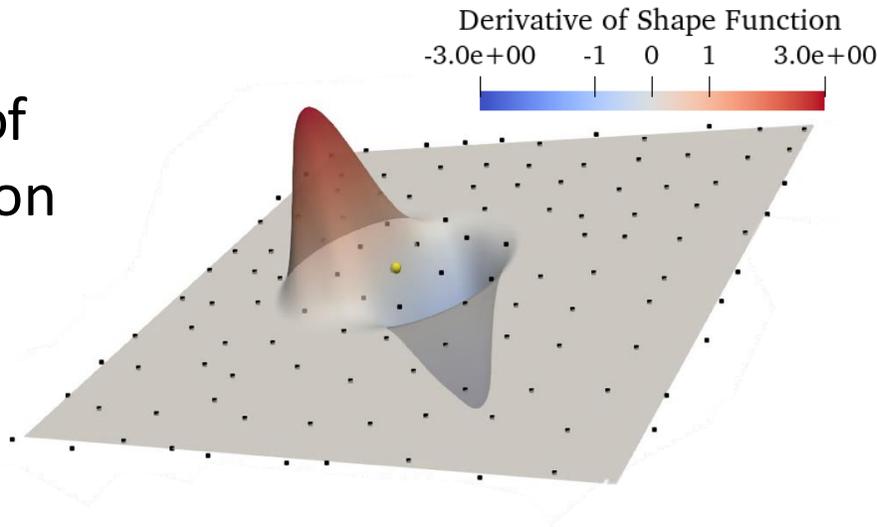
Interpolated shape function

$$\hat{\Psi}_I(\mathbf{x}) = \mathbf{M}_{Ij} N_i(\mathbf{x})$$



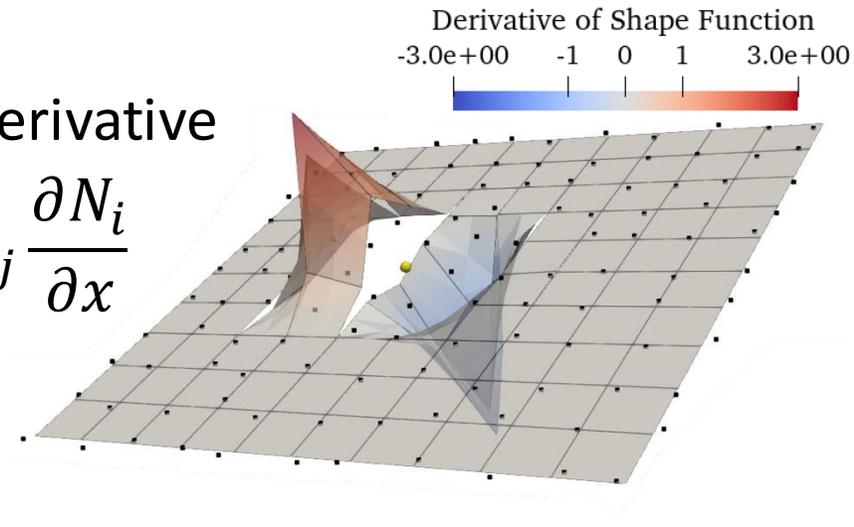
Derivative of shape function

$$\frac{\partial \Psi_I}{\partial x}$$



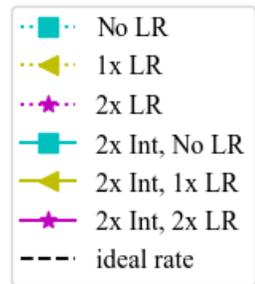
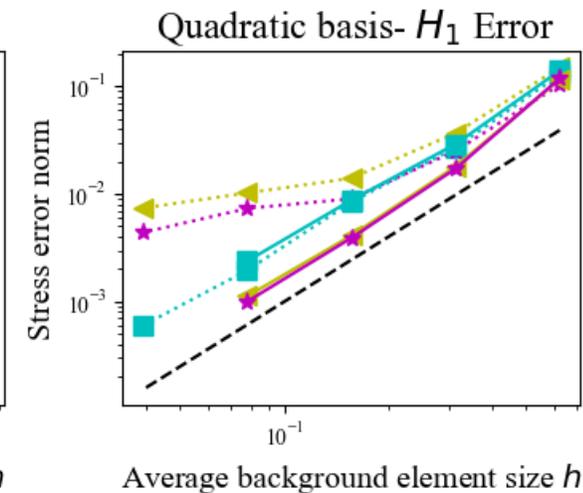
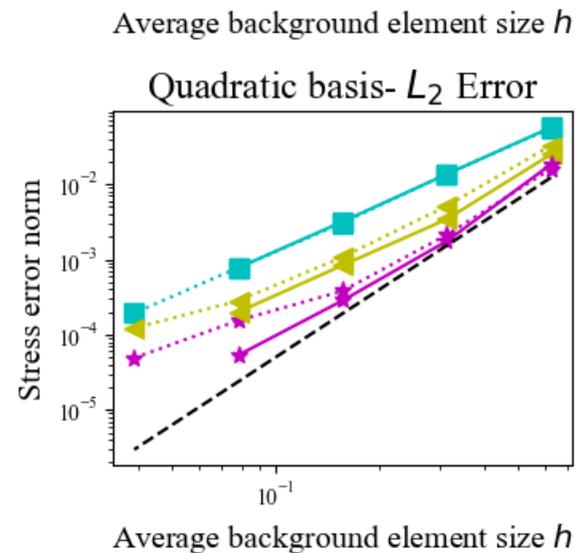
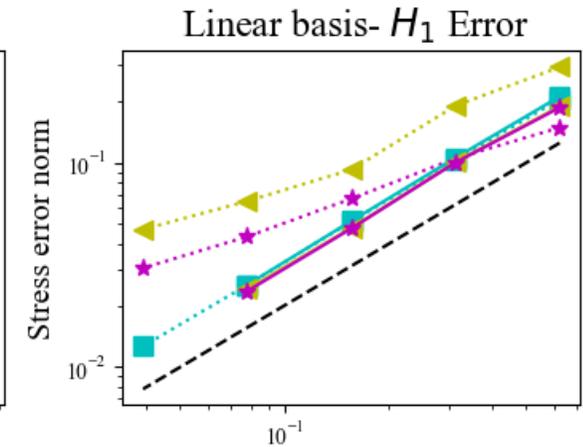
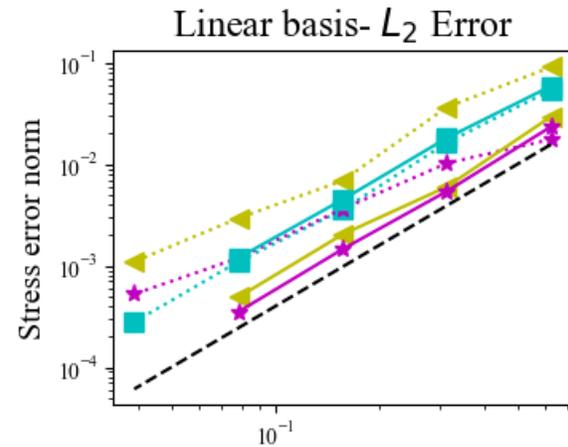
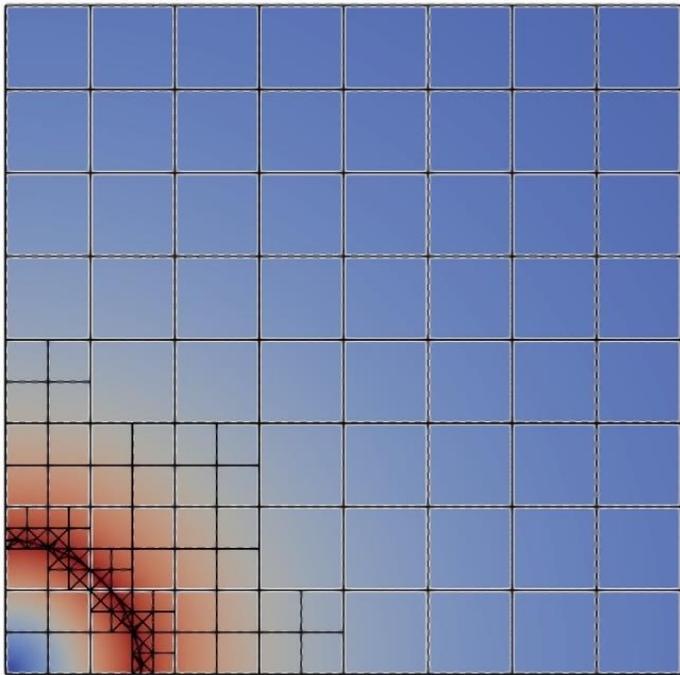
Interpolated derivative

$$\frac{\partial \hat{\Psi}_I}{\partial x} = \mathbf{M}_{Ij} \frac{\partial N_i}{\partial x}$$



Int-RKPM analysis of multi-material problems with enrichment and local refinement

Linear-elasticity problem with a circular inclusion and induced eigenstrain



Part 7:

Useful Links

Useful Links

- EXHUME (MORIS) software library

<https://github.com/kkmaute/moris>

- FEniCS implementation of interpolation-based immersed analysis:

<https://github.com/jefromm/interpolation-based-immersed-fea>

- First paper on interpolation-based immersed analysis:

J.E. Fromm, N. Wunsch, R. Xiang, H. Zhao, K. Maute, J.A. Evans, and D. Kamensky.
"Interpolation-based immersed finite element and isogeometric analysis."
CMAME 405 (2023): 115890.

<https://doi.org/10.1016/j.cma.2023.115890>

MORIS



*FEniCS
Implementation*



Useful Links

- [Slides and videos from Fall 2023 EXHUME Collaborators Workshop](#)



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