

The Development of the EM RF-Edge Interactions Mini-app “Stix” Using MFEM

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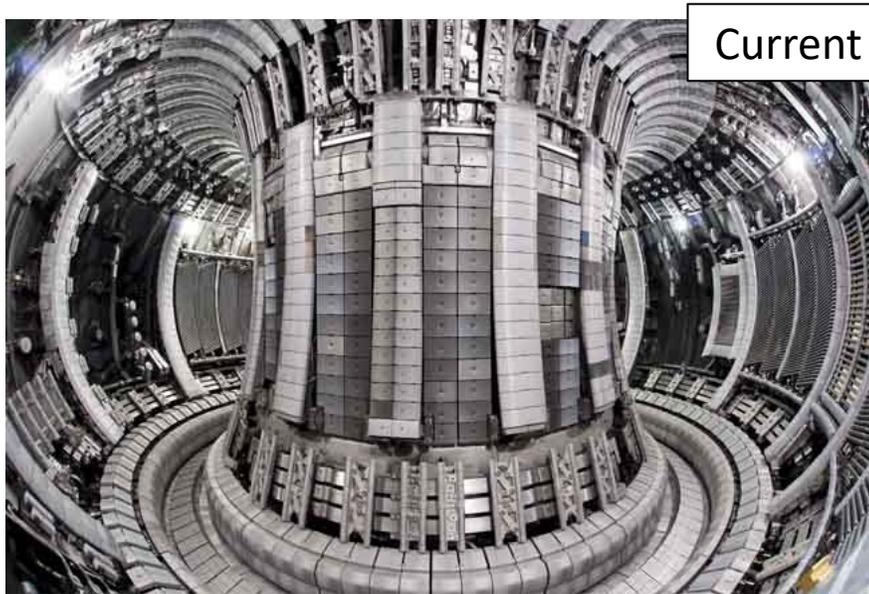
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Ion cyclotron radio frequency (ICRF) power is important in heating in fusion devices

Tokamaks need external heating to reach fusion relevant temperatures

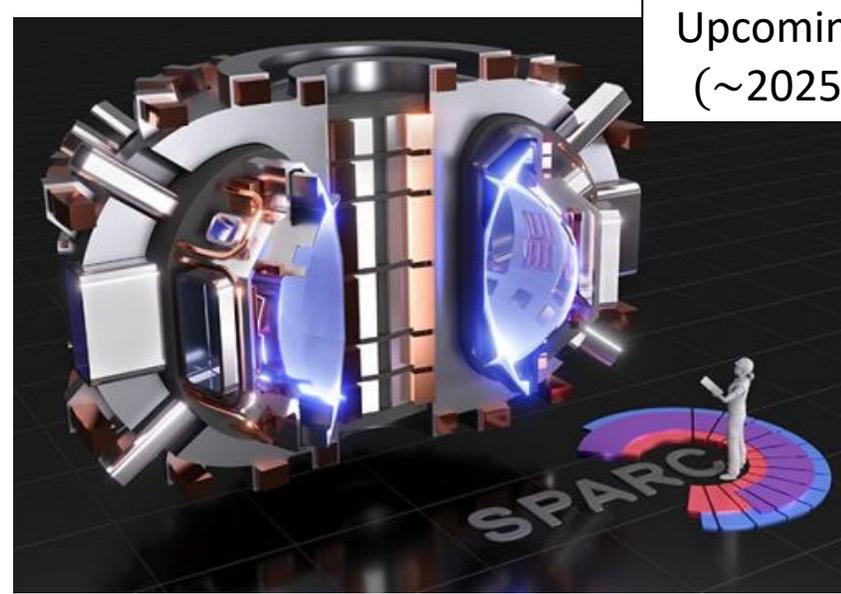
- RF waves are common method to use
- Advantages of the ICRF regime ($\sim 20 - 100$ MHz) include:
 - Efficient
 - Cost effective
 - Well established technology

Current and future machines use significant ICRF heating



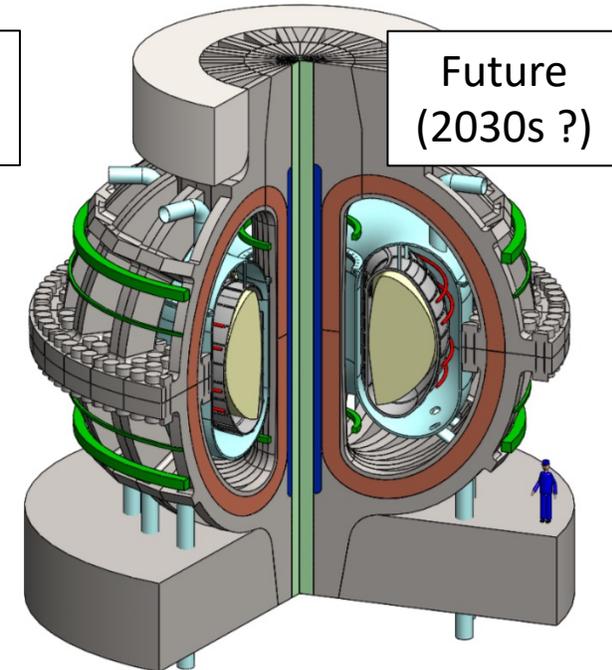
Current

JET ~ 6 MW



Upcoming
(~ 2025)

SPARC ~ 25 MW



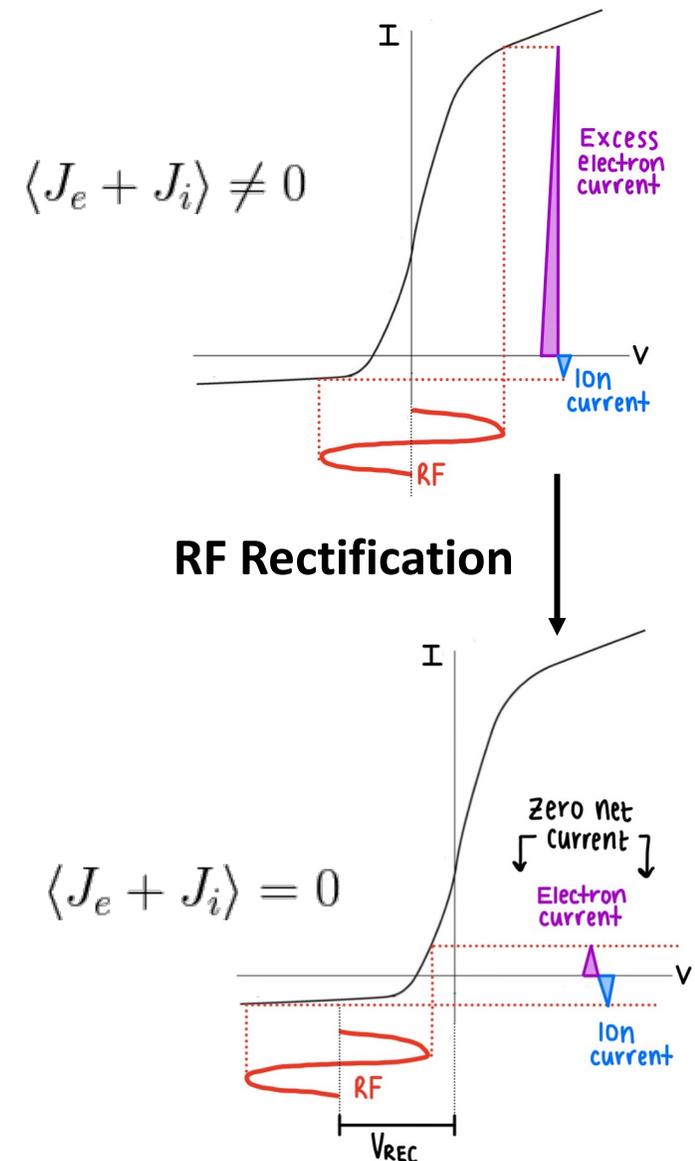
Future
(2030s ?)

ARC ~ 13.6 MW

[B.N. Sorbom et al. 2015]

ICRF power produces large rectified potentials that influence adverse effects

- **Problem:** ICRF power produces rectified sheath potentials (~ 100 s of Volts) that damage PFCs due to impurity generation and hot spots
- Path to longer pulsed fusion makes these effects increasingly important to predict and model
- Numerically modeling rectified sheaths will help to understand:
 - **Where** they form
 - What factors **influence** larger rectification
 - Ways to engineer methods of **mitigation** of sputtering and hot spots



Motivation for “Stix” Mini-app

- Need a RF simulation model that incorporates physics of RF sheath in global RF code
 - Because $\lambda_{ICRF} \gg \Delta$ (sheath thickness), sheath can be approximated as a BC
(~ cm) (~ mm)

- In the form of J. Myra et al. 2015:

$$E_t = \nabla_t (V_{sh}) = \nabla_t \left(\frac{\omega}{i} D_n z_{sh} \right) \quad \text{[J. Myra et al. PoP 2015]}$$

- Want a robust code framework to test different solvers and have the possibility of an **integrated model via impurity generation (RustBCA) and transport (MAPS) codes**
 - Result: cold plasma finite element RF solver - Stix1D and Stix2D mini-app built off the MFEM library

Physics Involved: the RF sheath BC

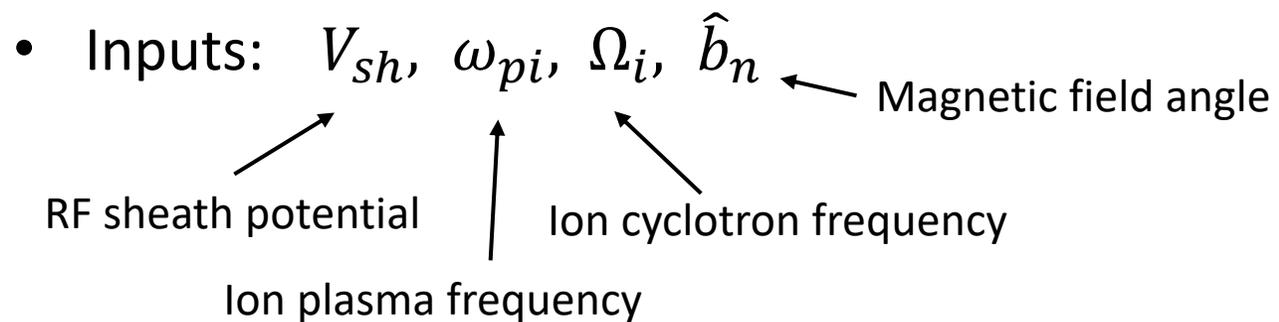
- The J. Myra et al. 2015 RF sheath boundary condition is given as:

Oscillating RF sheath potential (AC)

$$E_t = \nabla_t (V_{sh}) = \nabla_t \left(\frac{\omega}{i} D_n z_{sh} \right)$$

[J. Myra et al. PoP 2015]

- This BC couples the macro-scale global RF code to the micro-scale sheath physics encapsulated in the complex sheath impedance, z_{sh}
- z_{sh} is found through J. Myra 2017 parameterization code:



- V_{sh} is dependent on D_n making this BC non-linear

What is the Stix mini-app?

- Originally adapted from an EM mini-app solver

Solves for the magnetic field, \vec{H} , in the frequency domain using H(Curl) basis functions:

$$\nabla \times \vec{\epsilon}^{-1}(\nabla \times \vec{H}) - \omega^2 \mu_0 \vec{H} = \nabla \times \vec{\epsilon}^{-1} \vec{J}_{\text{ext}}$$

From \vec{H} , Stix computes: \vec{E} , \vec{D} , and \vec{S} (Poynting flux)

- Uses a cold plasma dielectric tensor:
 - There is the option to include a temperature profile that adds artificial dissipation into $\vec{\epsilon} \rightarrow \frac{i\nu}{\omega}$
- Is a 3D code but is run in pseudo-1D (Stix1D) and pseudo-2D (Stix2D)
 - 1D and 2D meshes are extruded into y-z and z directions
 - With periodicity in the respective extruded directions: set k_y , k_z in 1D and k_z in 2D
- Non-linear sheath BC implemented in a fixed-point iteration
 - The Minimal Polynomial Extrapolation (MPE) technique was also developed
 - Shown to converge in less iterations to the sheath solution
- Currently solves using direct solvers: SuperLU and MUMPS

Implementation of RF Sheath BC in Stix: $E_t = \nabla_t (V_{sh}) = \nabla_t \left(\frac{\omega}{i} D_n z_{sh} \right)$

- Idea is to have the non-linear sheath BC be solved at the same time as the H field:

Solved simultaneously are the:

1) Wave equation

$$\sum_j \left\{ \int_{\Omega} (\nabla \times \vec{W}_i) \cdot (\vec{\epsilon}^{-1} \nabla \times \vec{W}_j) d\Omega - \omega^2 \mu_0 \int_{\Omega} \vec{W}_i \cdot \vec{W}_j d\Omega + \int_{\partial\Omega} \vec{W}_i \cdot \underbrace{(\hat{n} \times \vec{\epsilon}^{-1} \nabla \times \vec{W}_j)}_{= E_t = \nabla_t (V_{sh})} d\Gamma \right\} \vec{H}_j = -i\omega \int_{\Omega} \vec{W}_i \cdot (\nabla \times \vec{\epsilon}^{-1} \vec{J}_{\text{ext}}) d\Omega$$

and

2) V_{RF} potential

$$V_{sh} = -i\omega D_n z_{sh} = -i\omega \hat{n} \cdot \left(\frac{\nabla \times \vec{H}}{-i\omega} \right) z_{sh} = \hat{n} \cdot (\nabla \times \vec{H}) z_{sh}$$

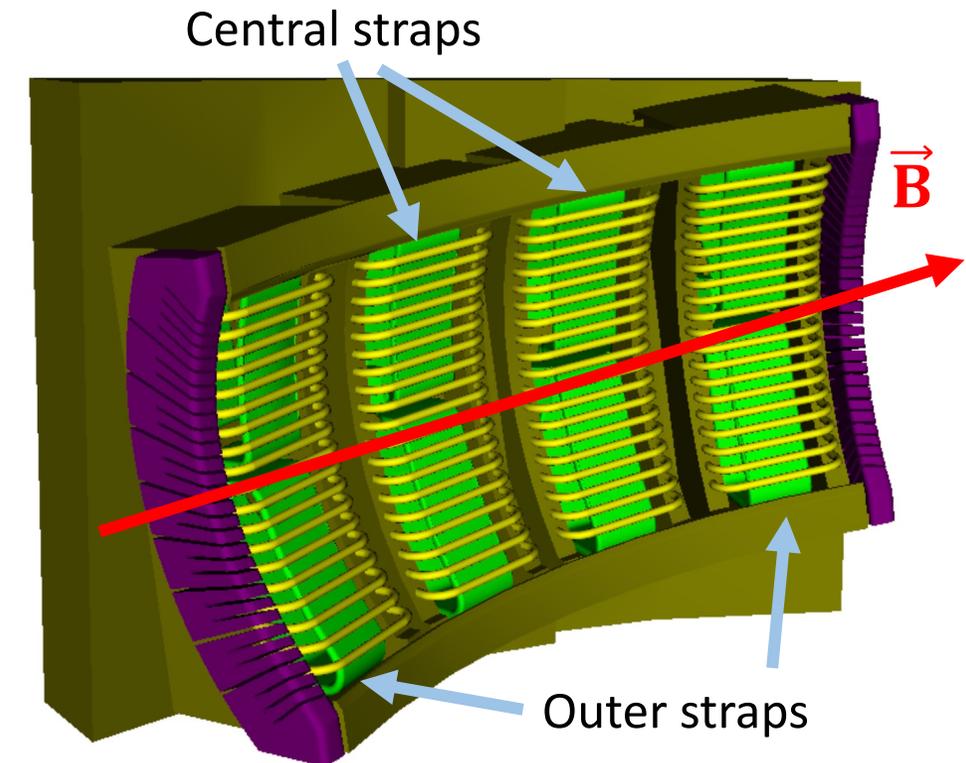
Found using J. Myra parameterization code [2]

- A block matrix is created using these equations
 - Using SuperLU the Schur complement is found for the wave equation block which is then used to solve the entire matrix iteratively using GMRES
- The code then iterates on the sheath impedance (z_{sh}) as a fixed-point iteration
- Once convergence criterion is met, currently set to $|\phi_n - \phi_{n+1}| < 10^{-3}$:
 - Code stops and writes out V_{RF} and V_{REC} (along with the EM fields)

Bridging simulation with experiment: Alcator C-Mod power phasing study

- Looked at how to mitigate impurities by optimizing the ICRF antenna design
- Ratio of power of central straps to the total power of the 4 straps ($P_{\text{cent}}/P_{\text{total}}$) was varied from ~ 0 to 1
 - Phasing: $[0 \pi 0 \pi]$
- Impurities and plasma potential on/close to the antenna were measured
- Motivation to use an integrated model approach for simulations:
 - Stix (potentials) + RustBCA (impurity fluxes)

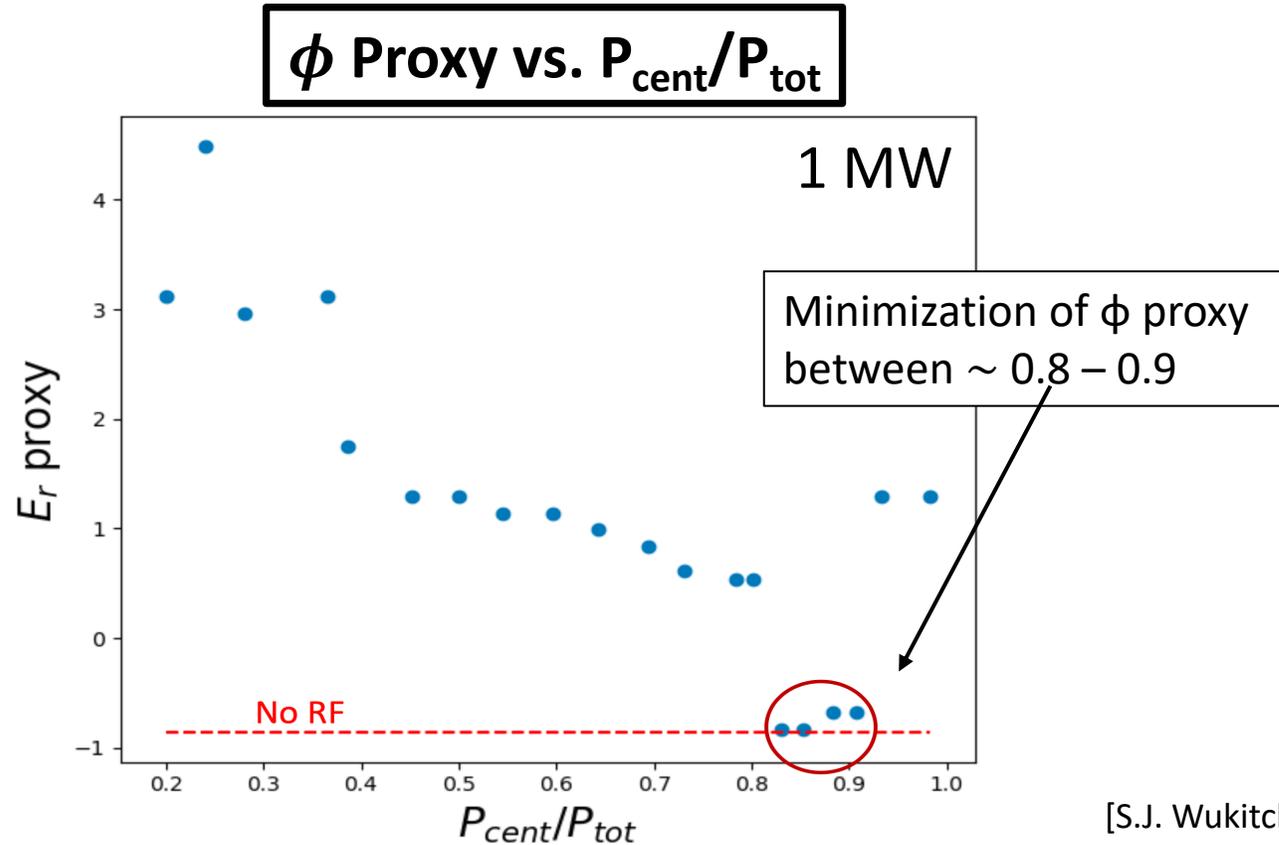
C-Mod's field aligned 4-strap ICRF antenna



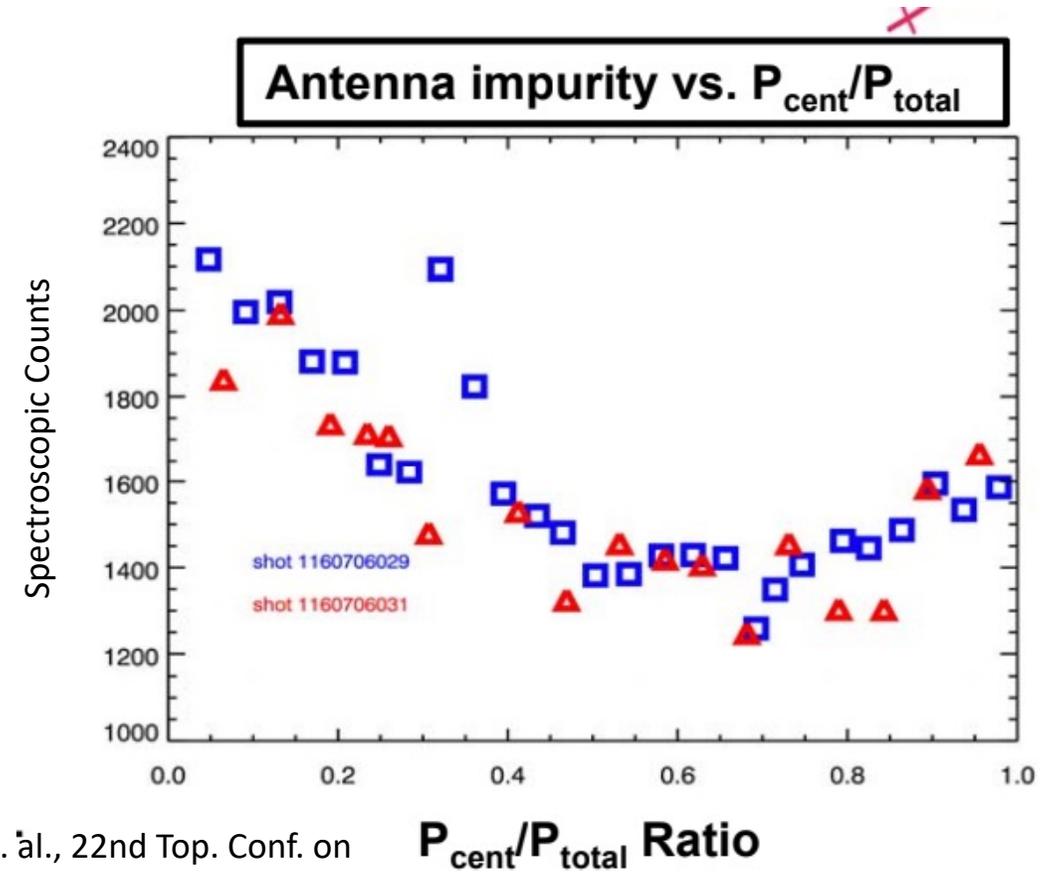
[Courtesy of Tom Jenkins, TechX]

Experiment found minimization of both impurities and potentials

- Antenna impurities were minimized for $P_{\text{cent}}/P_{\text{total}} \sim 0.5 - 0.9$ for 1 MW
- Sheath potential were minimized for $P_{\text{cent}}/P_{\text{total}} \sim 0.8 - 0.9$ for 1 MW
- Behavior believed to be due to the **image current cancelation** on the antenna box



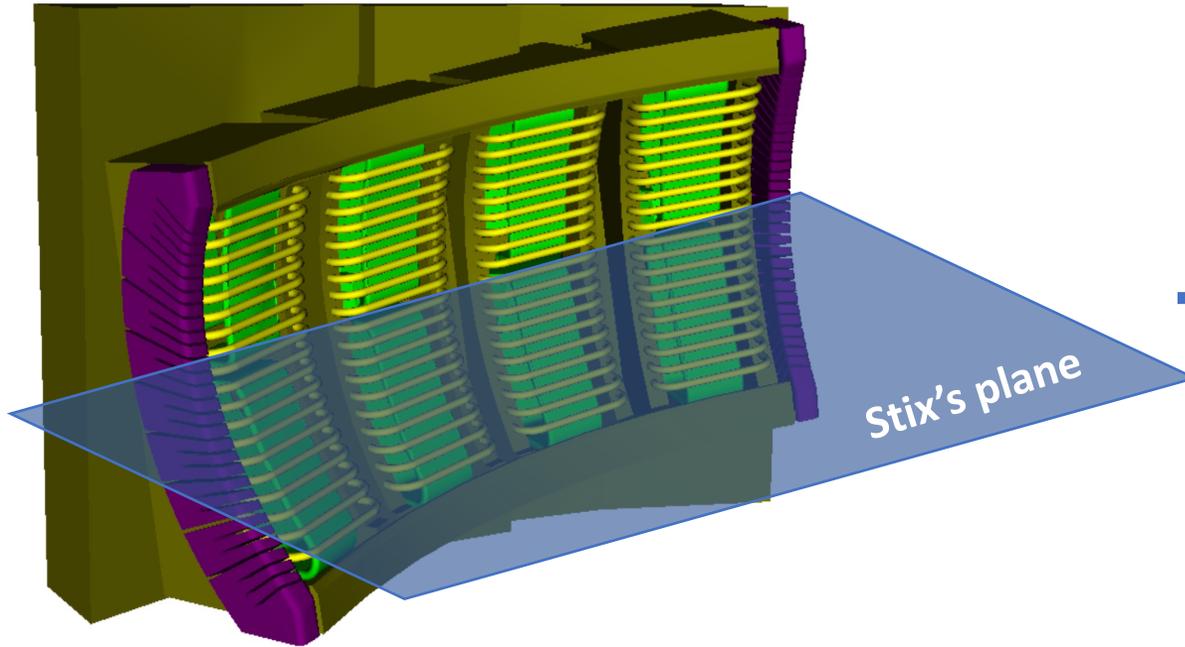
[Courtesy of R. Diab, MIT]



[S.J. Wukitch, et. al., 22nd Top. Conf. on Radio frequency Power in Plasmas (2017)]

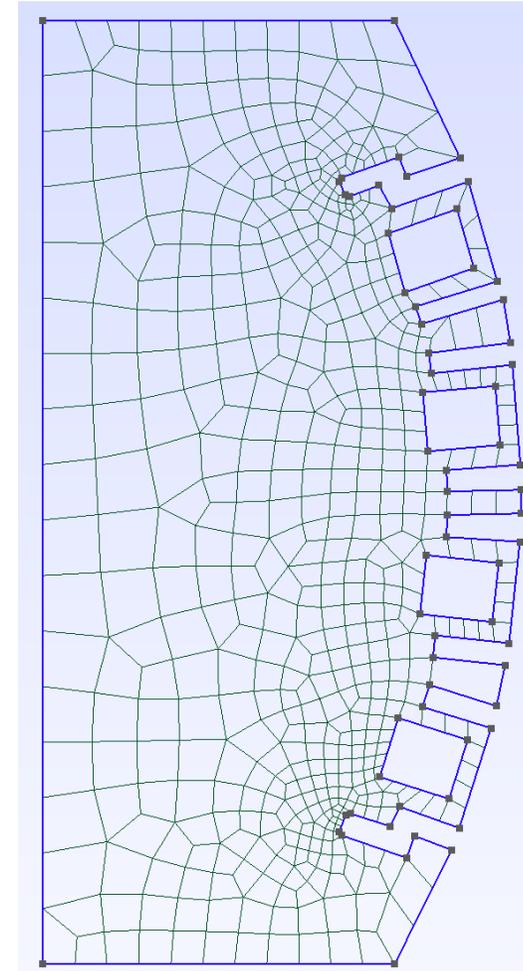
How does this C-Mod case look like computationally in Stix?

3D View of Domain:



[Courtesy of Tom Jenkins, TechX]

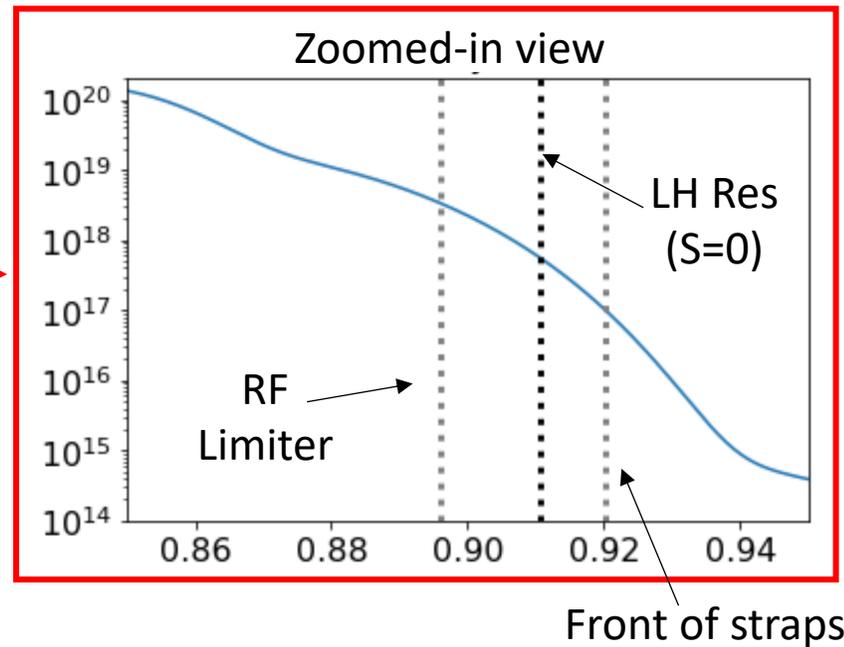
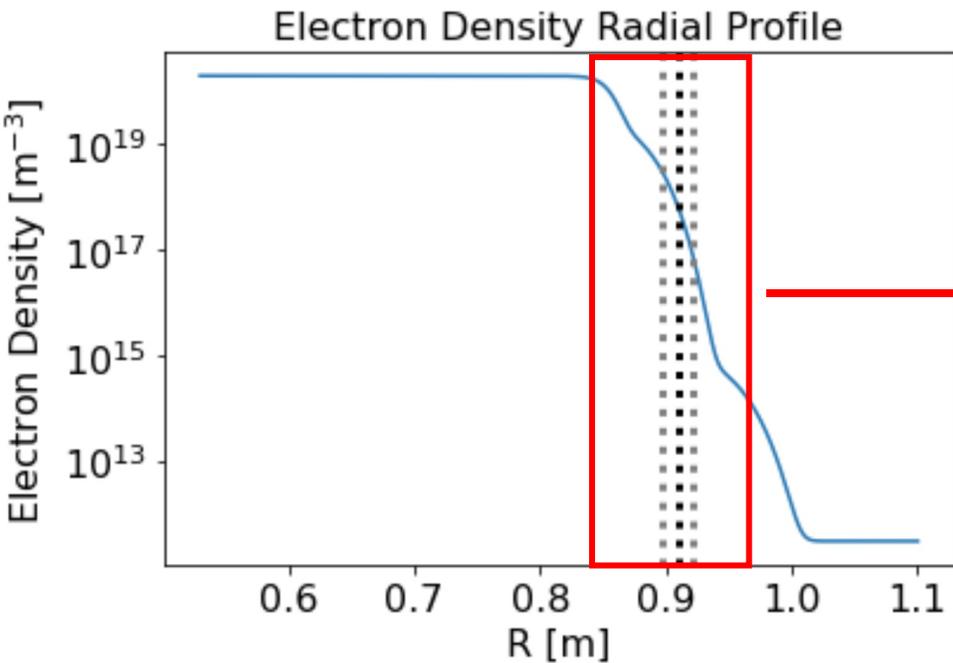
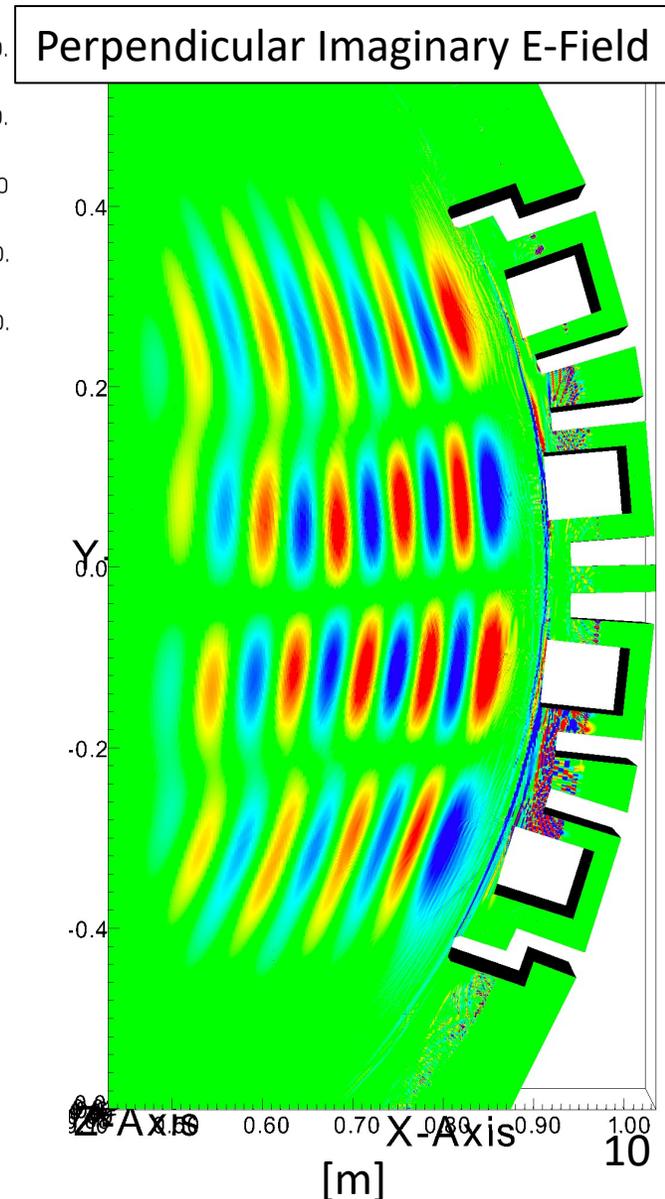
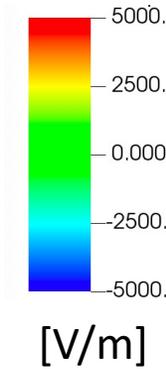
2D View of Domain: Stix's Mesh



[mesh before serial + AMR refinement]

Stix's simulation setup

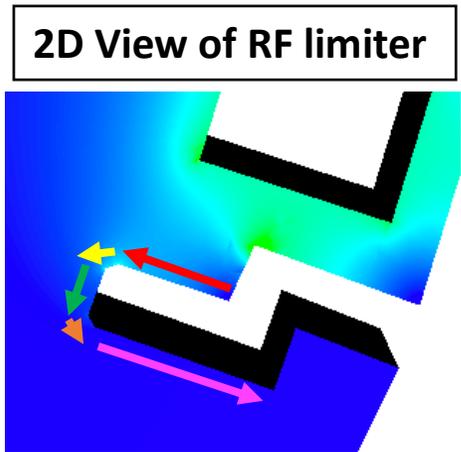
- EQDSK magnetic field from experiment
- $[0 \pi 0 \pi]$ antenna phasing
- Sheath BC along RF limiter edges
- Artificial collisional profile to damp waves propagating into the core
- Pedestal-like density profile:
 - $n_{e,\max} = 2 \times 10^{20} \text{ m}^{-3}$ and $n_{e,\min} = 1 \times 10^{11} \text{ m}^{-3}$
 - Exciting a parasitic SW in front of the straps



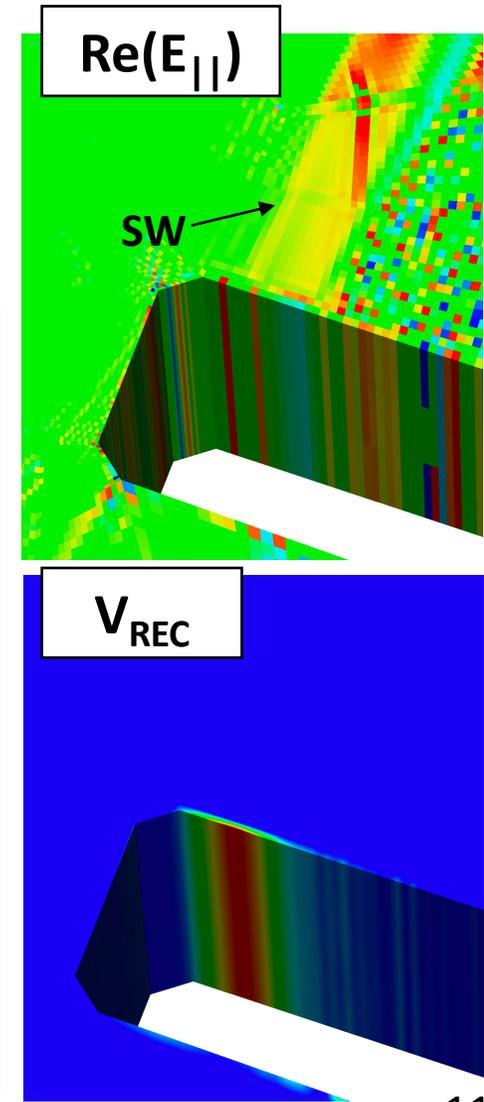
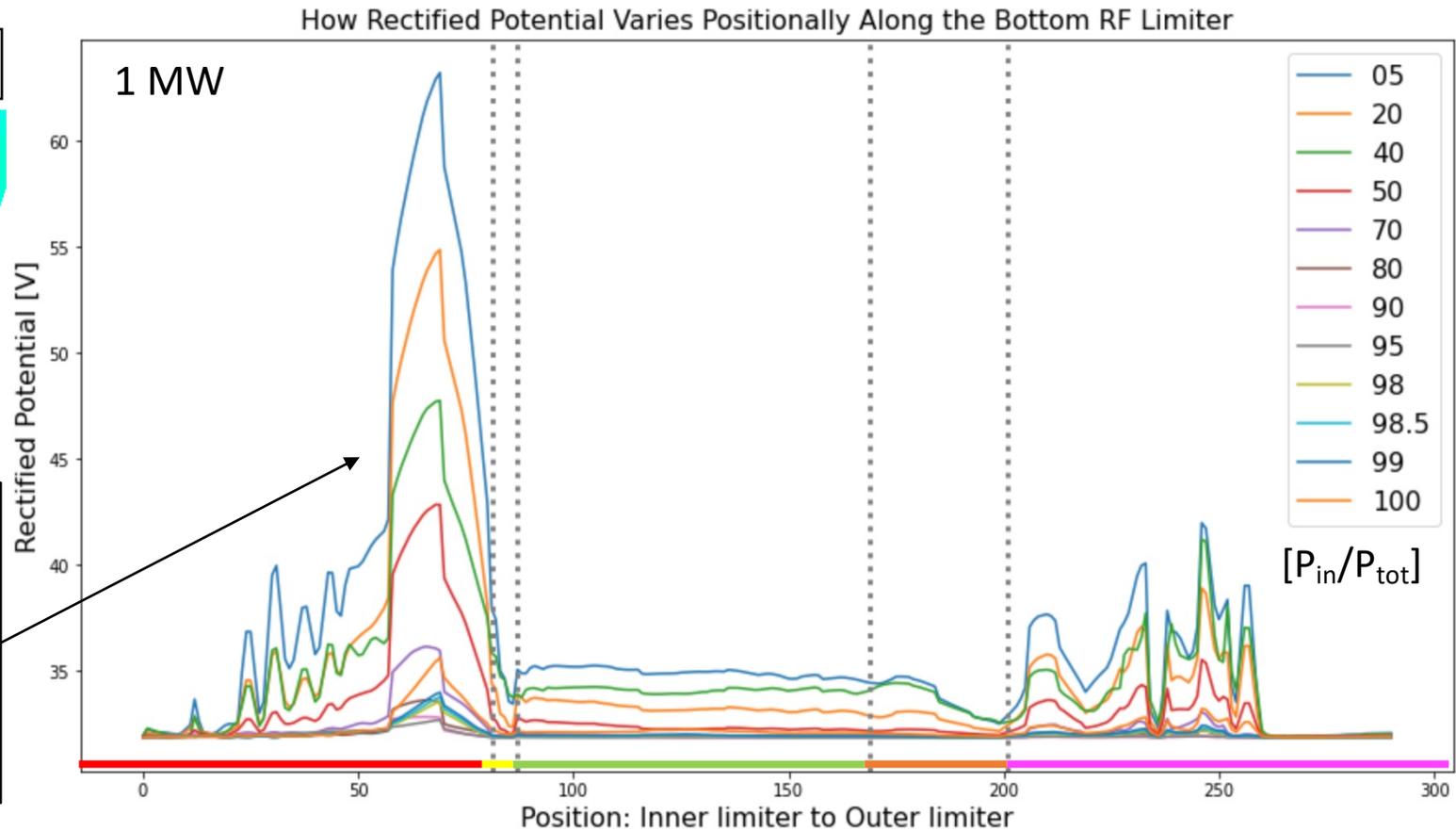
Front of straps

Stix's resulting rectified potentials

- Sheath BC was placed all along RF limiter
 - Found rectification only on inner facing limiter (red arrow)
- Rectification happened between densities of: $\sim 5.5 \times 10^{16} - 1.2 \times 10^{17} \text{ m}^{-3}$
 - Below the lower hybrid (LH) resonance which occurs at $5.4 \times 10^{17} \text{ m}^{-3}$
 - RF sheath caused by propagating slow wave (SW)

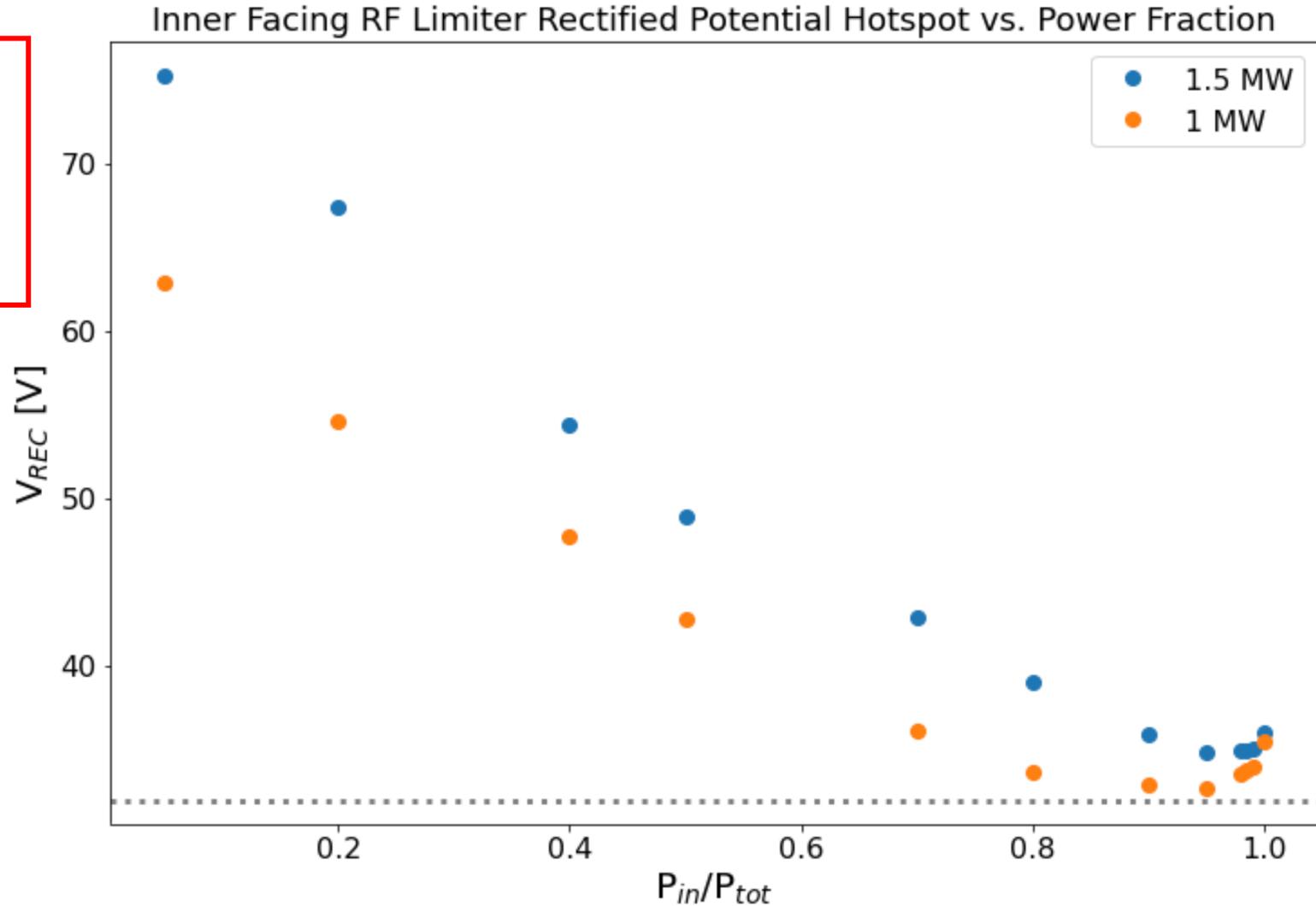


Largest rectification occurs on inner facing RF limiter closest to the plasma

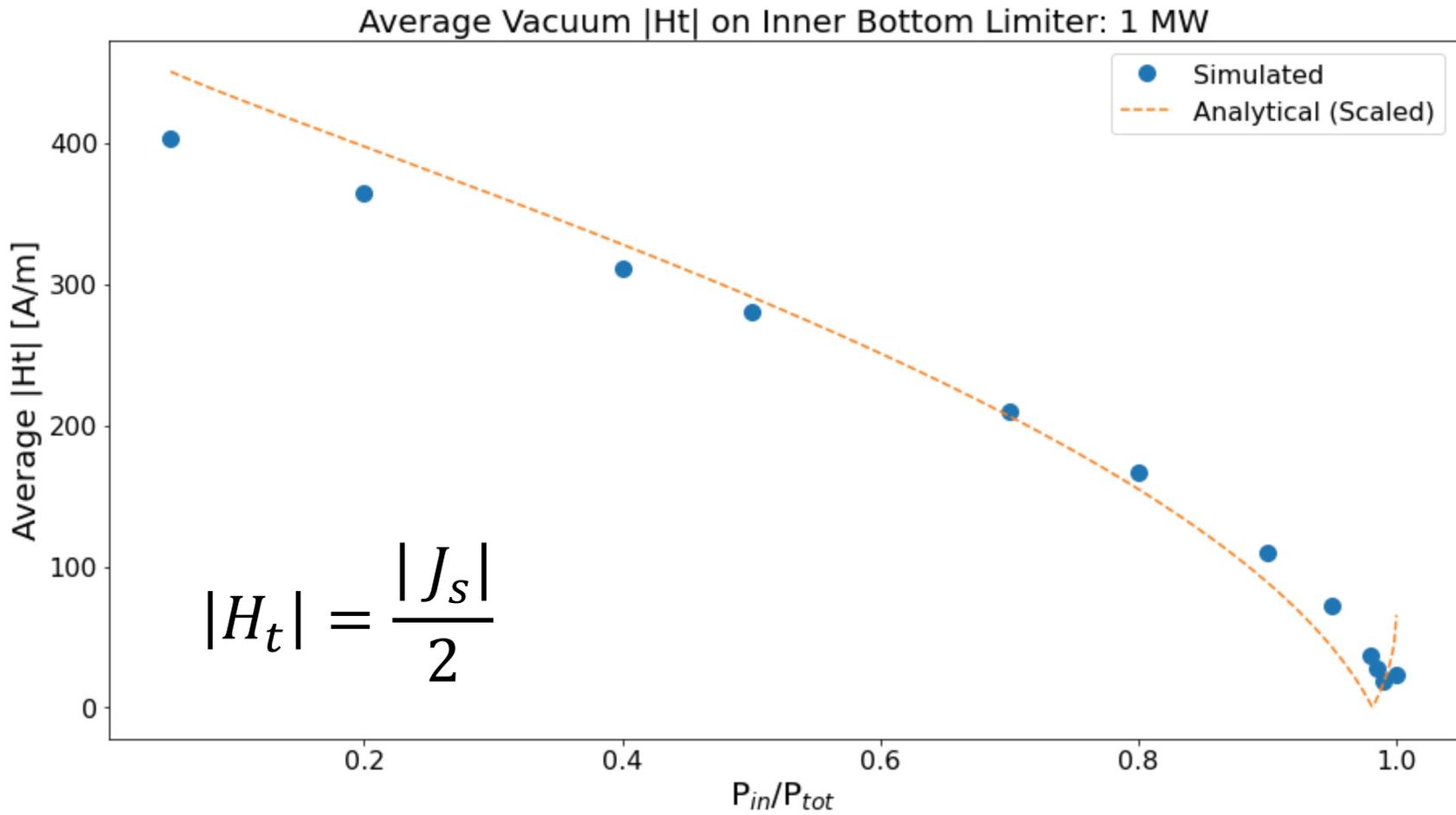


Stix's rectified potentials vs. power phasing scan finds the same trend as in experiment

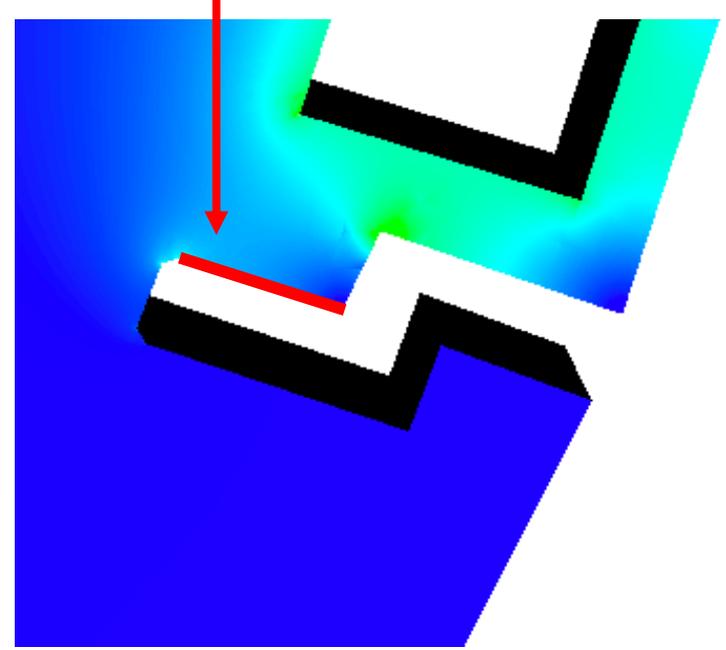
- Found V_{REC} minimized between:
 - $P_{cent}/P_{tot} \sim 0.8 - 0.95$ for 1 MW
 - $P_{cent}/P_{tot} \sim 0.9 - 1.0$ for 1.5 MW
- Minimum is pushed to a higher power fraction for high antenna power
- 1.5 MW doesn't reach Bohm sheath at minimum like 1 MW does
- Edge profiles are kept constant for both power scans



Vacuum power scanning shows minimum surface current at higher fraction P_{cent}/P_{tot} at 0.99 on inner RF limiter



Area of interest



This suggests that the slow wave (SW) shifts the image current cancelation to a lower power fraction from 0.99 to $\sim 0.8 - 0.95$ for 1 MW

Summary

- A new cold-plasma finite element RF solver called “Stix” has been developed which couples a RF sheath BC to a global wave solve
- An experimental power-phasing study done with the 4-strap C-Mod antenna showed minimization of the rectified potentials at $P_{\text{cent}}/P_{\text{tot}} \sim 0.8 - 0.9$ for 1 MW
 - Antenna impurities were similarly minimized but for a broader range of $P_{\text{cent}}/P_{\text{tot}} \sim 0.5 - 0.9$
- 2D slice of the 4-strap C-Mod antenna was simulated using Stix to find the rectified potentials on the nearby RF limiters scanning $P_{\text{cent}}/P_{\text{tot}}$ from 0.05 to 1.0

The key takeaways:

- Stix showed:
 - A propagating SW was the source of the rectification in the simulation
 - **The same trend of minimization of the rectified potentials at $P_{\text{cent}}/P_{\text{tot}} \sim 0.8 - 0.95$ for 1 MW**
- Vacuum scans of the same domain show a minimization of the image currents at $P_{\text{cent}}/P_{\text{tot}} \sim 0.99$
 - **Suggests that the SW pushes the image current cancelation to a lower power fraction**

Future work:

- Integrated model:
 - Use Stix's V_{REC} as an input to an impurity flux code like RustBCA
- 3D simulation of antenna:
 - Preliminarily 3D simulations of ICRF multi-strap antennas suggest that there is a lot of variation of the rectified potential poloidally along the RF limiter
 - Strongest near the corners of the antenna box: shown in vacuum scans in COMSOL via image current cancelation